

CDM-MP81-A01

Draft Methodological tool

TOOL09: Determining the baseline efficiency of thermal or electric energy generation systems

Version 04.0

DRAFT



United Nations
Framework Convention on
Climate Change

COVER NOTE

1. Procedural background

1. The Executive Board of the CDM (hereinafter referred as the Board) at its ninety-fourth meeting (EB 94 report, para. 32) requested the Methodologies Panel (MP) to update default efficiency factors in the methodological tool "TOOL09: Determining the baseline efficiency of thermal or electric energy generation systems" (hereinafter referred as 'tool') on a regular basis (i.e. every two or three years), based on publicly available information.
2. Based on this mandate the MP, at its 79th meeting, started the work. At its 80th meeting, the MP agreed to seek public input on the work related to update the default efficiency factors for thermal energy generation, for grid-connected and off-grid power generation as provided in table 1 to table 3 of the Appendix 1 of the tool.
3. One stakeholder provided input to the public call. The comments received and its analysis is presented in Appendix 2 of this document. The MP has analysed the comments received and agreed to recommend the draft revised version of the tool for Board's approval.

2. Purpose

4. The present work confirms that the default efficiency factors as provided in the Appendix 1 of the tool are the latest valid values as referred from the publicly available literature sources.

3. Key issues and proposed solutions

5. The secretariat conducted a literature review to compare default efficiency factors from the tool against efficiency factors as reported in the literature. Table 1 to table 6 provide comparison of default efficiency factors between those reported in the literature and the current version of the tool.
6. In case of thermal applications, the MP recommends maintaining the default efficiency factors in the current version of the tool as the values are conservative. Except in the case of coal fired boiler, a change is proposed. Refer to table 1 for further details and the citation of the source for the literature review.

Table 1. Default efficiency factor for thermal application

| Technology of the energy generation system | Efficiency (in percentage) as reported in literature ¹ | Default efficiency factor (in percentage) as in current version of the tool | Default efficiency factor (in percentage) recommended |
|---|---|---|---|
| Natural gas fired boiler (w/o condenser) | 85.7 | 92 | 92 |
| Oil fired boilers adapted as Natural gas fired boiler (w/o condenser) | 80.6 | 87 | 87 |
| Oil fired boiler | 89.6 | 90 | 90 |
| Biomass fired boiler (on dry biomass basis) | 80.0 | 85 | 85 |
| Coal fired boiler | 90.3 | 80 | 90 |
| Other | NA | 100 | 100 |

7. In case of coal-based power generation, the MP recommends using conservative default efficiency factors among the one reported in the literature and current version of the tool. Refer to table 2 for further details.

Table 2. Default efficiency factor for coal-based power generation

| Technology type and region | Efficiency (in percentage) as reported in literature (LHV) ² | | | Default efficiency factor (in percentage) as in current version of the tool | Default efficiency factor (in percentage) recommended |
|---------------------------------|---|------|------|---|---|
| | 2015 | 2020 | 2030 | | |
| Steam Coal - SUBCRITICAL | | | | | |
| Europe | 39 | 39 | 39 | 39 | 39 |
| United States | 39 | 39 | 39 | | |
| Japan | 39 | 39 | 39 | | |
| Russia | 39 | 39 | 39 | | |
| China | 37 | 37 | 37 | | |
| India | 36 | 36 | 36 | | |
| Middle East | 37 | 37 | 37 | | |
| Africa | 35 | 35 | 35 | | |
| Brazil | 39 | 39 | 39 | | |

¹ IEA ETSAP - Technology Brief I01 <<https://iea-etsap.org/index.php/energy-technology-data/energy-supply-technologies-data>>.

² Unless otherwise mentioned, the default values are referred from IEA, Energy technology perspective, 2017, IEA, Projected costs of generating electricity, 2015 and IEA, World Energy Outlook, 2018.

| Technology type and region | Efficiency (in percentage) as reported in literature (LHV) ² | | | Default efficiency factor (in percentage) as in current version of the tool | Default efficiency factor (in percentage) recommended |
|--|---|------|------|---|---|
| | 2015 | 2020 | 2030 | | |
| Steam Coal - SUPERCRITICAL | | | | | |
| Europe | 43 | 43 | 43 | 45 | 45 |
| United States | 43 | 43 | 43 | | |
| Japan | 43 | 43 | 43 | | |
| Russia | 43 | 43 | 43 | | |
| China | 41 | 41 | 41 | | |
| India | 40 | 40 | 40 | | |
| Middle East | 41 | 41 | 41 | | |
| Africa | 39 | 39 | 39 | | |
| Brazil | 43 | 43 | 43 | | |
| Steam Coal - ULTRASUPERCRITICAL | | | | | |
| Europe | 45 | 46 | 47 | 50 | 50 |
| United States | 45 | 46 | 47 | | |
| Japan | 45 | 46 | 47 | | |
| Russia | 45 | 46 | 47 | | |
| China | 44 | 45 | 46 | | |
| India | 40 | 41 | 42 | | |
| Middle East | 43 | 44 | 45 | | |
| Africa | 41 | 42 | 43 | | |
| Brazil | 45 | 46 | 47 | | |
| Coal based IGCC | | | | | |
| Europe | 44 | 45 | 47 | 50 | 50 |
| United States | 44 | 45 | 47 | | |
| Japan | 44 | 45 | 47 | | |
| Russia | 44 | 45 | 47 | | |
| China | 43 | 44 | 46 | | |
| India | 41 | 42 | 44 | | |
| Middle East | 42 | 43 | 45 | | |
| Africa | 40 | 41 | 43 | | |
| Brazil | 44 | 45 | 47 | | |
| CFB³ | | | | | |

³ IFSA 2014, Industrial Fluidization South Africa, Glenburn Lodge, Cradle of Humankind, 19–20 November 2014, 'The value proposition of circulating fluidized-bed technology for the utility power sector', by R. Giglio and N. J. Castilla.

| Technology type and region | Efficiency (in percentage) as reported in literature (LHV) ² | | | Default efficiency factor (in percentage) as in current version of the tool | Default efficiency factor (in percentage) recommended |
|----------------------------|---|------|------|---|---|
| | 2015 | 2020 | 2030 | | |
| | 43.3 | | | 40 | 43 |
| PFB | | | | | |
| | 45 | | | 45 | 45 |

8. In case of combined-cycle gas-based power generation and reciprocal gas engines, the MP noted that the default efficiency factor in the current version of the tool is conservative when compared with the one reported in the literature. The MP recommends retaining the default efficiency factors in the current version of the tool except for open-cycle gas-based power generation. Refer to table 3 for further details.

Table 3. Default efficiency factor for gas-based power generation

| Technology type and region | Efficiency (in percentage) as reported in literature (LHV) ⁴ | | | Default efficiency factor (in percentage) as in current version of the tool | Default efficiency factor (in percentage) recommended |
|--|---|------|------|---|---|
| | 2015 | 2020 | 2030 | | |
| Combined Cycle Gas Turbine (CCGT) | | | | | |
| Europe | 59 | 59 | 60 | 62 | 62 |
| United States | 59 | 59 | 60 | | |
| Japan | 59 | 59 | 60 | | |
| Russia | 57 | 57 | 58 | | |
| China | 57 | 57 | 58 | | |
| India | 56 | 56 | 57 | | |
| Middle East | 57 | 57 | 58 | | |
| Africa | 58 | 58 | 59 | | |
| Brazil | 58 | 58 | 59 | | |
| Open Cycle Gas Turbine (OCGT) | | | | | |
| Europe | 40 | 40 | 41 | 42 | 44 |
| United States | 40 | 40 | 41 | | |
| Japan | 40 | 40 | 41 | | |
| Russia | 38 | 38 | 39 | | |

⁴ Refer to footnote 2.

| Technology type and region | Efficiency (in percentage) as reported in literature (LHV) ⁴ | | | Default efficiency factor (in percentage) as in current version of the tool | Default efficiency factor (in percentage) recommended |
|--|---|------|------|---|---|
| | 2015 | 2020 | 2030 | | |
| China | 38 | 38 | 39 | | |
| India | 38 | 38 | 39 | | |
| Middle East | 38 | 38 | 39 | | |
| Africa | 38 | 38 | 39 | | |
| Brazil | 38 | 38 | 39 | | |
| Belgium | 44 | | | | |
| Germany | 40 | | | | |
| New Zealand | 30 | | | | |
| United Kingdom | 39 | | | | |
| Reciprocal gas engine⁵ | | | | | |
| | 27 – 42 | | | 48.5 | 48 |

9. In case of oil-based reciprocal engines, the MP recommends retaining default efficiency factor, while in case of oil-based steam turbines, recommends using the default efficiency factor as mentioned in the current version of the tool as it is conservative over the one reported in literature. Refer to table 4 for further details.

Table 4. Default efficiency factor for oil-based power generation

| Technology type and region | Efficiency (in percentage) as reported in literature ⁶ | Default efficiency factor (in percentage) as in current version of the tool | Default efficiency factor (in percentage) recommended |
|----------------------------|---|---|---|
| Steam turbine | | | |
| | 42 | 44 | 44 |
| Reciprocal engine | | | |
| | 48 | 48.5 | 48 |

⁵ Catalog of CHP technologies, section 2 – Technology Characterization – Reciprocating Internal Combustion Engines, US EPA, Combined heat and power partnership, March 2015.

⁶ Based on US EPA data, converted to LHV of fuel.

10. In case of biomass-based integrated gasification combined cycle power generation, the MP recommends using the default efficiency factors as reported in the literature and, in case of biomass-based steam turbine recommends retaining the current value. Refer to table 5 for further details.

Table 5. Default efficiency factor for biomass-based power generation

| Technology type and region | Efficiency (in percentage) as reported in literature (LHV) ⁷ | | | Default efficiency factor (in percentage) as in current version of the tool | Default efficiency factor (in percentage) recommended |
|------------------------------------|---|------|------|---|---|
| | 2015 | 2020 | 2030 | | |
| Biomass based IGCC | | | | | |
| | 35 | 38 | 42 | 40 | 42 |
| Biomass based steam turbine | | | | | |
| | 30 | 33 | 35 | 35 | 35 |

11. In case of co-generation, the MP recommends retaining default efficiency factor value as in the tool, except in the case of combined cycle-based cogeneration, it recommends the default efficiency factor value as reported in the literature. Refer to table 6 for further details.

Table 6. Default efficiency factor for co-generation

| Technology type and region | Efficiency (in percentage) as reported in literature (LHV) ⁸ | | | Default efficiency factor (in percentage) as in current version of the tool | Default efficiency factor (in percentage) recommended |
|----------------------------|---|------|------|---|---|
| | 2015 | 2020 | 2030 | | |
| Steam turbine | | | | | |
| Europe | 70 | 70 | 70 | 83.5 | 83 |
| United States | 70 | 70 | 70 | | |
| Japan | 70 | 70 | 70 | | |
| Russia | 70 | 70 | 70 | | |
| China | 70 | 70 | 70 | | |
| India | 70 | 70 | 70 | | |
| Middle East | 70 | 70 | 70 | | |
| Africa | 70 | 70 | 70 | | |
| Brazil | 70 | 70 | 70 | | |
| CCGT – CHP | | | | | |
| Europe | 82 | 82 | 83 | 78.8 | 83 |
| United States | 82 | 82 | 83 | | |
| Japan | 82 | 82 | 83 | | |
| Russia | 80 | 80 | 81 | | |

⁷ Refer to footnote 2.

⁸ Refer to footnote 3.

| Technology type and region | Efficiency (in percentage) as reported in literature (LHV) ⁸ | | | Default efficiency factor (in percentage) as in current version of the tool | Default efficiency factor (in percentage) recommended |
|---|---|------|------|---|---|
| | 2015 | 2020 | 2030 | | |
| China | 80 | 80 | 81 | | |
| India | 79 | 79 | 80 | | |
| Middle East | 80 | 80 | 81 | | |
| Africa | 81 | 81 | 82 | | |
| Brazil | 81 | 81 | 82 | | |
| Reciprocal engine⁹ | | | | | |
| | 77 - 83 | | | 88.8 | 89 |
| Microturbine (up to 500 kW)¹⁰ | | | | | |
| | 63 - 71 | | | 77.7 | 78 |

12. Further, the MP also reviewed the default efficiency factors for off-grid power plants and recommends maintaining the current values as provided in the tool. Refer table 7 for further details.

Table 7. Default efficiency factor for power plants with capacity up to 1000 kW

| Generation Technology | Nominal capacity of power plants (CAP, in kW) | | | | | |
|---|---|-----------|------------|-------------|-------------|--------------|
| | CAP≤10 | 10<CAP≤50 | 50<CAP≤100 | 100<CAP≤200 | 200<CAP≤400 | 400<CAP≤1000 |
| Reciprocal engine system (e.g. diesel-, fuel oil-, gas-engines) ¹¹ | 28% | 33% | 35% | 37% | 39% | 42% |
| Gas turbine systems ¹² | 28% | 32% | 34% | 35% | 37% | 40% |
| Small boiler/steam/turbine system ¹³ | 7% | 7% | 7% | 7% | 7% | 7% |

13. The MP noted that the tool is not applicable in case of use of fuel mix. However, it recommends that the tool should be made applicable for equipment that uses fuel mix and, in such cases, the efficiency of the energy generating equipment is based on the highest efficiency of the fuel used, that constitute more than 10% of the fuel used.

⁹ Refer footnote 6 and Implementing EPA's Clean Power Plan: A Menu of Options <http://www.4cleanair.org/NACAA_Menu_of_Options>.

¹⁰ Refer footnote 3.

¹¹ Based on diesel consumption data available at <https://www.dieselserviceandsupply.com/Diesel_Fuel_Consumption.aspx>.

¹² Refer footnote 6 and Implementing EPA's Clean Power Plan: A Menu of Options <http://www.4cleanair.org/NACAA_Menu_of_Options>.

¹³ Factsheet from the US DoE: available at <https://www.energy.gov/sites/prod/files/2016/09/f33/CHP-Steam%20Turbine.pdf>.

14. Further, the MP recommends differentiation of categorisation of the power generating equipment based on the capacity of the equipment rather than whether it is grid-connected or off-grid. Simplification is also suggested by rounding-off the default efficiency factor values to the nearest integer, for example, 83.7 will be round-off to 84 and 90.3 will be round-off to 90.

4. Impacts

15. The proposed draft revised tool, if approved, will have updated default efficiency factors for technology used, for thermal energy generation, and for grid-connected and off-grid power generation purpose.

5. Subsequent work and timelines

16. No subsequent work is envisaged for this item.

6. Recommendations to the Board

17. The MP recommends that the Board adopts the draft revised version of the tool.

7. References

- (a) IEA, Energy technology perspective, 2017
- (b) IEA, Projected costs of generating electricity, 2015
- (c) IEA, World Energy Outlook, 2018
- (d) IEA ETSAP - Technology Brief I01, May 2010
- (e) Catalogue of CHP technologies, section 2 – Technology Characterization – Reciprocating Internal Combustion Engines, US EPA, Combined heat and power partnership, March 2015.
- (f) Implementing EPA's Clean Power Plan: A Menu of Options, 2015
<http://www.4cleanair.org/NACAA_Menu_of_Options>
- (g) Factsheet from the US DoE: available at
<<https://www.energy.gov/sites/prod/files/2016/09/f33/CHP-Steam%20Turbine.pdf>>

| TABLE OF CONTENTS | Page |
|---|-------------|
| 1. INTRODUCTION | 11 |
| 2. SCOPE, APPLICABILITY, AND ENTRY INTO FORCE | 11 |
| 2.1. Scope | 11 |
| 2.2. Applicability | 11 |
| 2.3. Entry into force | 12 |
| 3. NORMATIVE REFERENCES | 12 |
| 4. DEFINITIONS | 12 |
| 5. PARAMETERS | 13 |
| 6. BASELINE METHODOLOGY PROCEDURE | 13 |
| 6.1. Option A: Use the manufacturer’s load-efficiency function | 14 |
| 6.2. Option B: Establish a load-efficiency function based on measurements and a regression analysis | 15 |
| 6.3. Option C: Establish the efficiency function based on historical data and a regression analysis | 17 |
| 6.4. Option D: Use the manufacturer’s efficiency values | 17 |
| 6.5. Option E: Determine the efficiency based on measurements and use a conservative value | 18 |
| 6.6. Option F: Use a default value | 19 |
| APPENDIX 1. DEFAULT EFFICIENCY FACTORS | 20 |
| APPENDIX 2. ANALYSIS OF COMMENTS | 22 |

1. Introduction

1. The tool provides methodological guidance to estimate efficiency of both thermal energy and power generation units.

2. Scope, applicability, and entry into force

2.1. Scope

2. The tool describes various procedures to determine the baseline efficiency of an energy generation system, for the purpose of estimating baseline emissions. The tool may be used in case of project activities that improve the energy efficiency of an existing system through retrofits or replacement of the existing system by a new system.
3. The tool provides different procedures to determine the baseline efficiency of the energy generation system: either a) a load-efficiency function is determined which establishes the efficiency as a function of the operating load of the system or b) the efficiency is determined conservatively as a constant value.

2.2. Applicability

4. This tool is applicable to energy generation systems that:
 - (a) Generate only electricity (and no thermal energy heat); or
 - (b) Produce only thermal energy (and no electricity); or
 - (c) Produce both electricity and thermal energy (cogeneration).
5. Also, the following conditions apply:
 - (a) The tool is not applicable to waste heat recovery systems to calculate efficiency values using options (A) to (E) as provided under paragraph 12 below;
 - (b) The tool can be applied only if load is the main operating parameter¹ that influences the efficiency of the energy generation system. For cogeneration systems, the heat to power ratio may also be considered a main operating parameter.
6. Methodologies referring to this tool should specify for which energy generation systems the tool is used and whether a load-efficiency function and/or a constant efficiency should be determined.

¹ In some of the project activities that implement energy efficiency improvements, the efficiency at a particular load point shall be compared between the baseline and project scenarios. In such situations load on the equipment is the main operating parameter that determines the efficiency and associated emissions. Other parameters such as steam pressure and temperature may also influence the efficiency, but for the purpose of this tool, the efficiency is assumed to be constant within the permitted variations specified by the manufacturer, e.g. within $\pm 5\%$ or $\pm 10^\circ\text{C}$.

2.3. Entry into force

7. The date of entry into force is the date of the publication of the **EB ##** meeting report on **DD month YYYY**.

3. Normative references

8. This tool refers to the following documents:
- (a) ASME PTC-4: Fired Steam Generators;
 - (b) ASME PTC-6: Steam Turbines;
 - (c) BS 845: Methods for assessing thermal performance of boilers for steam, hot water and high temperature heat transfer fluids;
 - (d) EN 12952-15: Water tube boilers and auxiliary installations - Part 15: Acceptance tests;
 - (e) IEC 60953-3: Rules for steam turbine thermal acceptance tests - Part 3: Thermal performance verification tests of retrofitted steam turbines.

4. Definitions

9. The definitions contained in the Glossary of CDM terms shall apply.
10. For the purpose of this tool, the following definitions also apply:
- (a) **Cogeneration plant** - a power-and-heat plant in which at least one heat engine simultaneously generates both heat and power;
 - (b) **Efficiency** - is defined as the net quantity of useful energy generated² by the energy generation system per quantity of energy contained in the fuel fired, **while considering its lower heating value**:
 - (i) In case of boilers that are used only for thermal energy generation (and not for power generation), the efficiency is defined as the net quantity of useful heat generated per quantity of energy contained in the fuel fired in the boiler;
 - (ii) In case of power plants producing only electric power (not cogeneration plants), the efficiency is defined as the net electricity generated by the power plant as a whole divided by the quantity of energy contained in the fuel fired;
 - (iii) In case of cogeneration plants, both definitions of efficiency **as above applies**, and overall efficiency is defined **of as** the sum of both efficiencies;

² Useful energy generated refers to useful energy supplied by the energy generating system. In the case of boilers that are used only for thermal energy generation (and not for power generation), the net quantity of useful energy corresponds to the enthalpy of the steam supplied by the boiler minus the enthalpy of the feed water, the enthalpy of any condensate return and the enthalpy of any boiler blow-down that is recovered. In case of power plants, the useful energy generated corresponds to the total quantity of electricity generated by the power plant minus the auxiliary electricity consumption of the power plant (e.g. for pumps, fans, controlling, etc.).

- (c) **Energy generation system or system** - the term *system* refers to a facility that generates electricity or thermal energy from combustion of fuels. In case of electricity generation, the term *system* refers to the entire power plant including all necessary equipment, such as boiler, turbine, and generator as well as auxiliary equipment such as fuel processing systems, water conditioning systems, cooling tower, etc. This could include steam turbine generators or gas turbine generators or combined cycle power plants. In case of thermal energy generation, the term system includes all systems that produce thermal energy, such as steam boilers, fluid heaters, etc. The term energy generation system should include all auxiliary equipment, such as the fuel processing system, the water conditioning system etc.;
- (d) **Load** - refers to the output (**power**) of the energy generation system at which the system is operated during efficiency determination tests. It is expressed in kW or MW;
- (e) **Load - Efficiency function** - a mathematical function representing the efficiency of the energy generation system as a function of the load;
- (f) **Performance curves** - are a graphical representation of the efficiency of the energy generation system at different loads and different operating conditions. For example, performance curves of a boiler illustrate the efficiency against load at different operating conditions, such as the steam pressure and temperature;
- (g) **Regression analysis** - a statistical method used to establish cause-effect for the investigation of relationships between the variables;
- (h) **Lower heating value (LHV)** - The heat produced by combustion of unit quantity of a solid or liquid fuel when burned, at a constant pressure of 1 atm (0.1 MPa), under conditions such that all the water in the products remains in the form of vapor.

5. Parameters

11. This tool provides procedures to determine the following parameters:

Table 1. Parameters

| Parameter | SI Unit | Description |
|-------------|---------------|--|
| η | Dimensionless | Efficiency of the energy generation system as a constant value |
| $\eta=f(L)$ | Dimensionless | Load-efficiency function expressing the efficiency of the energy generation system as a function of the load at which the system is operated |

6. Baseline methodology procedure

12. Project participants may use one of the following options to estimate the efficiency of the energy generation system:
- (a) Option A: Use the manufacturer's load-efficiency function;
- (b) Option B: Establish a load-efficiency function based on measurements and a regression analysis;

- (c) Option C: Establish the efficiency based on historical data and a regression analysis;
 - (d) Option D: Use the manufacturer's efficiency values;
 - (e) Option E: Determine the efficiency based on measurements and use a conservative value;
 - (f) Option F: Use a default value.
13. Options (A) to (E) are applicable only to energy generation systems that use a single fuel type³ and fuel mix including waste energy. In case of fuel mix, the efficiency of the energy generating equipment is calculated based on the fuel with highest percentage of share in a monitoring year in terms of calorific value.
14. Project participants should document which option is used to establish the efficiency of the relevant system, including, in the case of options (B), (C) or (E), the type of measuring equipment used, details of how the measurements were carried out and the measurement results.
15. For cogeneration projects, project participants shall also document and justify the choice of heat to power ratio used in the measurements.

6.1. Option A: Use the manufacturer's load-efficiency function

16. This option cannot be applied to determine a constant efficiency. The option can be used if:
- (a) The manufacturer of the energy generation system provided load-efficiency functions or performance curves for the system at the time of installation⁴; and
 - (b) If these functions or curves clearly show the efficiency of the system at all applicable loads and for the relevant range of operational conditions;⁵ and
 - (c) The functions or curves are consistent with the equipment/system characteristics; and
 - (d) If no retrofitting was done on the system prior to the implementation of the project activity that could have increased its efficiency.
17. The load-efficiency function of the energy generation system is derived from the manufacturer's function or curves, whereby each load point should have a corresponding

³—Options A to E are not applicable to systems that use multiple fuels or different qualities of fuel within the same fuel type. For example if the system uses coal of different grades (e.g. Grade A, B or I, II etc.) with significantly varying calorific values, these options cannot be used to determine the baseline efficiency, as different grades of coal may result in different efficiencies. However, a small quantity of auxiliary fuels may be used for start-ups, not exceeding 3% of the main fuel used in the equipment.

⁴—The highest value in 30 continuous operation days during the monitoring period shall be considered as representative value.

⁵ This option cannot be used if the manufacturer provided efficiency values only at discrete load points. Project participants may consider Option D in this case.

efficiency for the relevant operating conditions (e.g. pressure and temperature of the steam).

18. In the case of performance curves, project participants may either derive a mathematical function from the curve or develop a table with efficiency vs. load values. The mathematical function or the table should closely represent the manufacturer's performance curves.
19. If the manufacturer supplies a mathematical relationship, this relationship can be used directly to derive the baseline efficiency of the energy generation system for the relevant operating conditions (e.g. pressure and temperature of the steam).
20. This option is conservative because the actual efficiency of the energy generation system is generally lower than the efficiency at the time of installation, due to ageing and deterioration of system, unless the system is retrofitted during its service.

6.2. Option B: Establish a load-efficiency function based on measurements and a regression analysis

21. Establish the load-efficiency function by conducting efficiency tests on the energy generation system⁶ and applying a regression analysis on the test results. The efficiency tests shall be conducted following the guidance provided in relevant national/international standards⁷, such as ASME PTC-6, IEC 60953-3, ASME PTC-4 BS 845 or EN 12952-15 etc., preferably using direct methods (i.e. dividing the net output by the sum of all inputs). All measurements shall be conducted immediately after scheduled preventive maintenance has been undertaken and under favourable operation conditions.⁸ During the measurement campaign, the load should be varied over the whole operational range or the rated capacity of the energy generation system. The efficiency of the system should then be determined at different steady-state conditions. Document the monitoring procedures and results transparently. The tests shall be conducted by an independent entity such as the equipment supplier, sectoral experts/consultants etc. and the results of the efficiency tests shall be validated by the DOE.
22. Efficiency determination tests shall be conducted for the entire system as a whole including auxiliary equipment, such as the fuel conditioning system, preheating systems, etc. All energy inputs and outputs, such as the feed water supply or energy losses through blow down losses, shall be taken into consideration. Measurements shall be done for the complete system using calibrated equipment as required by the relevant national/international standards.

⁶ Tests shall be conducted before implementation of retrofits that are part of the project activity.

⁷ National/International Standards provides detailed procedures, methods, guidance and/or recommendations for system operation conditions, test conditions, recording of measurements, permissible variations in measurements, instrumentation, uncertainty management, etc. during performance/acceptance tests. The same guidance shall be applied as appropriate for conducting the measurements for efficiency determination under this tool.

⁸ Favorable operation conditions are optimal operation conditions, representative or favorable ambient conditions for the best efficiency of the energy generation system, including temperature and humidity, etc.

23. For the tests, two successive load points in the load range shall have an increment of at least 5% of the system's rated capacity. All efficiency tests shall be conducted for a predetermined discrete time interval as specified in standards. All tests shall be conducted for the same duration.
24. Each efficiency test provides a pair of data, i.e. (1) the load of the system and (2) the efficiency of system at that particular load. Based on the data collected at all load points, the load-efficiency function shall be established using a regression analysis. Project participants should choose the most suitable regression⁹ model such as linear, polynomial etc. following the general guidance given below:
- (a) Measure efficiency of the energy generation system at different load points as described above;
 - (b) Run a scatter plot, to determine the degree of the model. Identify the potential outliers to be filtered or re-run the test at that level to confirm the outlier. The fitting of higher-order polynomials of an independent variable with a mean not equal to zero can create complex multi-collinearity problems. Specifically, the polynomials will be highly correlated due to the mean of the primary independent variable. The correct sample size is critical to ensure a good representative curve is established. Take into account that polynomial models cannot be used for extrapolation;
 - (c) Determine the coefficient of the equation using any methodology but taking into account the recommendations in (b) above;
 - (d) The model should display:
 - (i) An ANOVA¹⁰ (Analysis of Variance) table showing the regression and residual sum of squares and the significance;
 - (ii) The coefficients table showing the **significance SIG**, these must be lower than 0.05.

Run a confirmatory data analysis, using the null hypothesis test to cover the entire population and allow forecasting for only the range of sample data.

Use α = probability (Reject Ho/Ho TRUE), a 0.05 value is recommended to assure the statistical significance.

⁹ For using regression analysis, necessary safeguards in order to ensure conservativeness and rigor of the fitted regression model should be used. In the process of fitting the regression, assumptions and requirements for regression models should be considered e.g. testing for multi-collinearity. It is recommended that project participants use the standard software for regression analysis and to determine the standard error.

¹⁰ In statistics, a result is called statistically significant if it is unlikely to have occurred by chance. "A statistically significant difference" simply means there is statistical evidence that there is a difference; it does not mean the difference is necessarily large, important, or significant in the common meaning of the word. The significance level of a test is a traditional statistical hypothesis testing concept. In simple cases, it is defined as the probability of making a decision to reject the null hypothesis when the null hypothesis is actually true (a decision known as a Type I error, or "false positive determination"). The decision is often made using the p-value: if the p-value is less than the significance level, then the null hypothesis is rejected. The smaller the p-value, the more significant the result is said to be.

- (e) The resultant load-efficiency function derived using regression model shall be adjusted for uncertainty in a conservative manner, by considering the upper bound values of the range at 95% confidence level at the load point where efficiency is to be derived.

6.3. Option C: Establish the efficiency function based on historical data and a regression analysis

- 25. This option can be used to determine a load-efficiency function or a constant efficiency.
- 26. The following conditions apply:
 - (a) In the case where the tool is used to establish a load-efficiency function, this option can only be used if measured data on the load and other parameters that are required to establish the efficiency of the system are available on an hourly basis (or a shorter time period) for the most recent year prior to the implementation of the project activity;
 - (b) In the case that the tool is used to establish a constant efficiency, this option can only be used if annual data on the efficiency of the energy generation system is available for the most recent three years prior to the implementation of the project activity;
 - (c) No retrofitting was done during the period for which historical data is used that could have increased the efficiency of the energy generation system. The historical data shall be the actual measured data such as flow, pressure, temperature, fuel consumption, energy outputs, etc. as applicable (e.g. from plant operational log books).
- 27. If the tool is used to establish a constant efficiency, the highest annual efficiency from the most recent three years should be chosen.
- 28. If the tool is used to establish a load-efficiency function, a regression analysis should be applied, following the guidance given under option b) above, using the historical data from the most recent year instead of conducting measurements on the system. The data pairs for load and efficiency should be used for the time interval at which they are available (one hour or, if available, for a shorter time interval).
- 29. Project participants shall document the complete data set used to establish the efficiency function.

6.4. Option D: Use the manufacturer's efficiency values

- 30. This option can be used to determine a constant efficiency.
- 31. The following conditions apply:
 - (a) If the manufacturer does not provide full load-efficiency functions or performance curves (if these functions are provided, Option A applies) but only the maximum efficiency at the optimal operating conditions;
 - (b) No retrofitting was done prior to implementation of the project that could have increased the efficiency of the energy system.

32. If these conditions are met, the efficiency provided by the manufacturer can be used as a conservative approach.

6.5. Option E: Determine the efficiency based on measurements and use a conservative value

33. This option can be used to determine a constant efficiency. Under this option, the efficiency of the energy generation system shall be measured based on performance tests before the implementing the project activity following national/international standards (e.g. ASME PTC-6, IEC 60953-3, ASME PTC-4, BS 845 or EN 12952-15 or other equivalent international and national standards), at discrete loads within the operation range or over the entire rated capacity, preferably using direct methods (i.e. dividing the net output by the sum of all inputs).
34. For tests, two successive load points in the load range shall have an increment of at least 5% of the system's rated capacity. At each load point one set of measurements shall be conducted. All efficiency tests shall be conducted for a same predetermined discrete time interval as specified in standards in the presence of an independent party (e.g. system manufacturer, technical consultant etc.).
35. All measurements shall be conducted immediately after scheduled preventive maintenance has been undertaken and under favorable operation conditions¹¹ (optimal operating conditions, representative or favorable ambient conditions for the best efficiency of the energy generation system, including temperature and humidity, etc.). During the measurement campaign, the load is varied over the whole operation range and the efficiency of the energy generation system is determined for different steady-state load levels. Document the measurement procedures and results transparently. A minimum of 10 measurements shall be taken at different loads in the full operation range or rated capacity and among the measurements, the highest efficiency shall be considered as a conservative approach.
36. Tests shall be conducted for the entire system including auxiliary equipment, such as the fuel conditioning system, preheating systems, etc. All energy inputs and outputs, such as the feed water supply or energy losses through blow down losses, shall be taken into consideration. Measurements shall be done using calibrated equipment as required by the relevant national/international standards.
37. Alternatively, if the efficiency test was conducted as part of concluding a previous retrofit activity¹² or energy audits or performance evaluation of the equipment, within 3 years prior to the implementation of the project activity and if the measurements and efficiency determination has already been verified and certified by an independent party, project participants may use the same data without conducting a new measurement campaign. This alternative is not applicable where a retrofit to increase the energy efficiency was done.

¹¹ Favorable operation conditions are optimal operation conditions, representative or favorable ambient conditions for the best efficiency of the energy generation system, including temperature and humidity, etc.

¹² Not part of the project activity.

38. Project participants shall justify and document the chosen optimal operating conditions.

6.6. Option F: Use a default value

39. This option can be used to determine a constant efficiency. Project participants may use the default values for the applicable technology from the appendix 1 as constant efficiency.¹³

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¹³ Project participants are encouraged to request for an amendment of this tool and may propose default values for technologies not covered in the table.

Appendix 1. Default efficiency factors

Table 1. Default efficiency factor for thermal applications

| Technology of the energy generation system | Default efficiency |
|---|--------------------|
| New n-Natural gas fired boiler (w/o condenser) | 92% |
| Old n-Oil fired boilers adapted as Natural gas fired boiler (w/o condenser) | 87% |
| New e-Oil fired boiler | 90% |
| New b-Biomass fired boiler (on dry biomass basis) | 85% |
| Old oil fired boiler | 85% |
| Old biomass fired boiler (on dry biomass basis) | 80% |
| Old e-Coal fired boiler | 80 90% |
| Other | 100% |

Table 2. Default efficiency factor for grid-connected power plants with installed capacity more than 1MW¹

| Grid power plant | | | |
|----------------------------|--------------------|-------------|---------------------|
| Generation technology | Commissioning year | | |
| | y≤2000 | 2000<y≤2012 | y>2012 ² |
| Coal | | | |
| Subcritical | 37% | 39% | 39% |
| Supercritical | - | 45% | 45% |
| Ultra-supercritical | - | 50% | 50% |
| IGCC | - | 50% | 50% |
| FBS | 35.5% | - | - |
| CFBS ³ | 36.5% | 40% | 40 43% |
| PFBS | - | 41.5% | 45% |
| Oil/n-Natural gas | | | |
| — Steam turbine | 37.5% | 39% | 44% |
| Reciprocal gas engine | 33% | 40% | 48.5 48% |
| Open cycle gas turbine | 30% | 39.5 39% | 42 44% |
| Combined cycle gas turbine | 46% | 60% | 62% |

¹ Values partially taken from the “Tool to calculate the emission factor for an electricity system”. Main sources for values are IEA Energy technology perspective publication 2010 to 2017, IEA, Projected costs of generating electricity, 2015 and IEA, World Energy Outlook, 2018.

² Main source for >2012 values: IEA energy technology perspectives from 2012: <<http://www.iea.org/publications/freepublications/publication/energy-technology-perspectives-2012.html>>.

³ IFSA 2014, Industrial Fluidization South Africa, Glenburn Lodge, Cradle of Humankind, 19–20 November 2014, ‘The value proposition of circulating fluidized-bed technology for the utility power sector’, by R. Giglio and N. J. Castilla.

| Grid power plant | | | |
|---------------------------------|-------|----------|-----|
| Oil | | | |
| Steam turbine | 37.5% | 39% | 44% |
| Reciprocal engine | 33% | 40% | 48% |
| Biomass⁴ | | | |
| IGCC | | 40-42% | |
| Other | | 35% | |
| Cogeneration⁵ | | | |
| Steam turbine | | 83.5-83% | |
| Gas turbine | | 78.8-83% | |
| Reciprocal engine | | 88.8-89% | |
| Mircoturbine (up to 500kW) | | 77.7-78% | |

Table 3. Default efficiency for off-grid power plants with installed capacity up to 1000 kW

| Generation Technology | Off-grid power plants | | | | | | |
|--|--|------------|-------------|--------------|--------------|---------------|----------|
| | Nominal capacity of power plants (CAP, in kW) | | | | | | |
| | CAP≤10 | 10<CAP ≤50 | 50<CAP ≤100 | 100<CAP ≤200 | 200<CAP ≤400 | 400<CAP ≤1000 | CAP>1000 |
| Reciprocal engine system (e.g. diesel-, fuel oil-, gas-engines) ⁶ | 28% | 33% | 35% | 37% | 39% | 42% | 45% |
| Gas turbine systems ⁷ | 28% | 32% | 34% | 35% | 37% | 40% | 42% |
| Small boiler/steam/turbine system ⁸ | 7% | 7% | 7% | 7% | 7% | 7% | N/A% |

⁴ Biomass calorific value is measured on dry basis. Maximum of 1% on energy basis fossil fuel co-firing is allowed, including start-up fuel. Main sources of values are IEA, Energy technology perspective, 2017, IEA, Projected costs of generating electricity, 2015 and IEA, World Energy Outlook, 2018. Main source for biomass values: IEA Energy Technology Essentials ETE03 <<http://www.leonardo-energy.org/sites/leonardo-energy/files/root/pdf/2008/essentials3%20-%20Biomass%20Power%20Gen.pdf>>.

⁵ The values are the overall efficiency, for electric efficiency, use the power-only default values. Main source for cogeneration values: Implementing EPA's Clean Power Plan: A Menu of Options <http://www.4cleanair.org/NACAA_Menu_of_Options> and IEA, Energy technology perspective, 2017, IEA, Projected costs of generating electricity, 2015 and IEA, World Energy Outlook, 2018.

⁶ Based on diesel consumption data available at https://www.dieselserviceandsupply.com/Diesel_Fuel_Consumption.aspx.

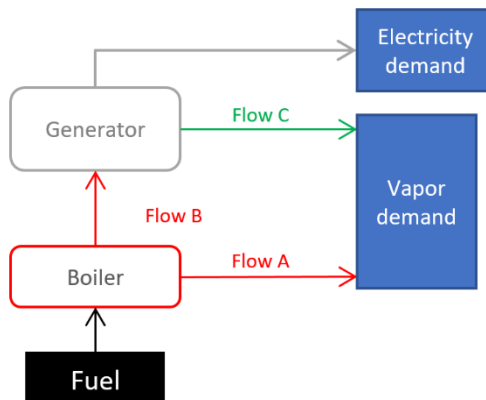
⁷ Refer footnote 6 and Implementing EPA's Clean Power Plan: A Menu of Options http://www.4cleanair.org/NACAA_Menu_of_Options.

⁸ Factsheet from the US DoE and available at: https://www.energy.gov/sites/prod/files/2016/09/f33/CHP_Steam%20Turbine.pdf.

Appendix 2. Analysis of comments

| 0 | 1 | 2 | 3 | 4 | 5 | 6 |
|---|---|------------------|---|--|---|---|
| # | Para No./ Annex / Figure / Table | Line Number | Type of comment ge = general te = technical e d = editorial | Comment (including justification for change) | Proposed change (including proposed text) | Assessment of comment (to be completed by UNFCCC secretariat) |
| 1 | Section 2.2 | 5. (a) | ge | Projects of energy efficiency can be done in a waste energy generator that is not part of another CDM project. | Allow the application of the tool in cases where the project is a retrofit of a waste energy generator. | The Meth Panel agreed to extend the scope of the tool to cover waste energy generators while efficiency is calculated using option A to option E. |
| 2 | Section 4 | 10. (b) (iii) | te | The definition of efficiency and the way to calculated is too general and doesn't cover a case that is really complex, like an extraction steam turbine. | There is an annex, that suggest a conservative way of calculation of thermal and electrical efficiency. | The Meth Panel agreed not to include procedure to calculate efficiency for multiple extraction turbines as the tool deals with the standard equipment that are available in the market and not with the tailor-made equipment with combinations of steam extraction. |
| 3 | Section 6.1 | Foot note 4 | ge | Why it is necessary to test during 30 days, if the curve is already constructed by the manufacturer? | | The Meth Panel agreed with the stakeholder to remove the requirement to use highest value in 30 continuous operation days during the monitoring period as manufacturer's curve provides highest value for an equipment. |
| 4 | Section 6.2 | 24. (d) (i) | ed | It is written ANOVA ⁹ | Eliminate the 9 | The typo error is corrected the in draft version of the tool. |
| 5 | Section 6.2 | 24. (d) (ii) | ge | What is the meaning of the acronym SIG? | | The typo error is corrected the in draft version of the tool. |
| 6 | Section 6.2 | Foot note 10 | ge | This foot note corresponds to a quick explanation of the concept, but it is not enough to describe correctly the concept. | May be evaluate the possibility to redirect to a source that explains in more detail. | The Meth Panel thinks this footnote is sufficient in context of its use in this tool. However, in case of further explanation on case-by-case basis the stakeholder may refer to related information available on internet. |

ANNEX: Efficiency for cogeneration in extraction steam turbines



Ratio of steam production: It is used to associate a specific quantity of fuel to a unit of vapor generated in the boiler.

$$R_{steam} = \frac{Volume\ of\ vapor}{Fuel_{in}} = \frac{F_A + F_B}{Fuel_{in}}$$

| | | |
|-------------|---|---|
| R_{steam} | = | Ratio of steam production. (kg of steam/m3 of fuel) |
| F_A | = | Mass of steam in the stream A (kg of steam) |
| F_B | = | Mass of steam in the stream B (kg of steam) |
| $Fuel_{in}$ | = | Total fuel feed to the boiler (m3 of fuel) |

Then, the ratio of steam production is used to estimate the equivalent in fuel of the vapor extracted from the turbine (flow C). This is not an accurate measure, because it considers vapor as it is coming directly from the boiler, but is a conservative approach, because the energy content in the extracted vapor is less than in the boiler outlet vapor.

$$Fuel_C = \frac{F_C}{R_{steam}}$$

| | | |
|----------|---|--|
| $Fuel_C$ | = | Equivalent of fuel to generate vapor in the flow stream C (m ³ of fuel) |
| F_C | = | Mass of steam in the stream C (kg of steam) |

Efficiency of heat production: Is the relationship between heat produced and the associated fuel used for the production of that energy.

$$\eta_{heat} = \frac{Energy_{flowA} + Energy_{flowC}}{Fuel\ energy\ content_{for\ vapor\ generation}}$$

$$\eta_{heat} = \frac{F_A * (h_A - h_{in} - h_{condensate} - h_{blow-down}) + F_C * (h_A - h_C - h_{condensate} - h_{blow-down})}{\left(Fuel_{in} - \frac{F_B}{R_{steam}} + \frac{F_C}{R_{steam}}\right) * NCV}$$

| | | |
|------------------|---|--|
| η_{heat} | = | Efficiency of heat production |
| h_{in} | = | Enthalpy of the feed water (TJ/kg) |
| h_A | = | Enthalpy of the flow stream A (TJ/kg) |
| $h_{condensate}$ | = | Enthalpy of any condensate (TJ/kg) |
| $h_{blow-down}$ | = | Enthalpy of any boiler blow-down (TJ/kg) |
| h_C | = | Enthalpy of the flow stream C (TJ/kg) |
| NCV | = | Net Calorific Value (TJ/m ³) |

Efficiency of electricity production: Is the amount of electricity produced vs the amount of fuel equivalent to the steam flow B that enters the turbine.

$$\eta_{elec} = \frac{E_{elec}}{\left(\frac{V_B}{R_{steam}}\right) * NCV}$$

| | | |
|---------------|---|--------------------------------------|
| η_{elec} | = | Efficiency of electricity production |
| E_{elec} | = | Electric energy generated (TJ) |

Document information

| Version | Date | Description |
|---------|------------------|--|
| 04.0 | 2 March 2020 | MP 81, Annex 1 To be considered by the Board at EB 106. The draft version of this document (CDM-MP80-A10) was available for public input from 11 to 25 October 2019. It received one input. Revision to update the default efficiency factor values for thermal energy and electrical energy generating equipment. |
| 03.0 | 9 October 2019 | MP 80, Annex 10 A call for input will be issued for this draft document. Revision to update the default efficiency factor values for thermal energy and electrical energy generating equipment. |
| 02.0 | 27 November 2015 | EB 87, Annex 11 Revision to: <ul style="list-style-type: none"> Expand the tool to include cogeneration; Include default values for cogeneration and biomass technologies. |

CDM-MP81-A01

Draft Methodological tool: TOOL09: Determining the baseline efficiency of thermal or electric energy generation systems

Version 04.0

| <i>Version</i> | <i>Date</i> | <i>Description</i> |
|----------------|--------------|--------------------------------------|
| 01.0 | 17 July 2009 | EB 48, Annex 12 Initial adoption. |

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