



**CLEAN DEVELOPMENT MECHANISM
PROJECT DESIGN DOCUMENT FORM (CDM-PDD)
Version 03 - in effect as of: 28 July 2006**

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Abbreviations

CIGAR	Covered In-Ground Anaerobic Reactor
COD	Chemical Oxygen Demand
GHG	Greenhouse gas
IRR	Internal rate of return
SQS	Siam Quality Starch Company Limited

**SECTION A. General description of project activity.****A.1 Title of the project activity:**

Siam Quality Starch Wastewater Treatment and Energy Generation Project in Chaiyaphum, Thailand (the Project)

Version 1.3 18/12/2008

A.2. Description of the project activity:

Siam Quality Starch Company Limited (SQS) manufactures Native and Modified Starch, extracted and refined from tapioca root, at its starch factory in Chaiyaphum Province, in the North Eastern region of Thailand. The production of starch, totalling about 200,000 tonnes annually, produces a large amount of high organic content wastewater, which emits methane when treated in anaerobic open lagoons prior to land application in eucalyptus plantations that surround the lagoons, on-site.

The Project, to be carried out by SQS at its starch factory, is the installation and operation of an anaerobic digestion and methane recovery system for the treatment of wastewater coupled with an energy generation system. In the absence of the Project, the wastewater will be treated in a series of anaerobic open lagoons, emitting methane during the long decomposition process. The captured methane will be destructed in boilers totalling 17.068MW_{th} for the production of hot thermal oil for use in heating air in process dryers.

The Project will therefore be responsible for two types of emission reductions. The first is the avoidance of methane, a potent greenhouse gas (GHG), that would be emitted from the baseline open lagoons, through its capture and destruction. The second is the displacement of bunker oil by the Project's carbon neutral energy, which will result in the reduction of carbon dioxide emissions from the combustion of bunker oil. The project activity is expected to reduce GHGs by an average of about 100,000 tonnes annually.

The Project contributes to sustainable development of Thailand in the following ways:

- Improvement of local air quality. Apart from the reduction in GHGs, the Project will improve the environmental performance of SQS's starch factory by reducing the COD load of effluent entering the open lagoons. Organic effluent treated in open lagoons not only emits a large amount of methane, a flammable gas, but also produces a strong pungent stench. By using the captured methane for energy generation and reducing fossil fuel consumption, the Project will also reduce emissions associated with the burning of fossil fuels.
- Reduction in reliance of fossil fuels. The project activity will displace internal bunker oil consumption. While the Project's fossil fuel consumption is small as compared to power plants, it is nevertheless significant in that the replication of such projects nation-wide will amount to a large reduction in the long term.

**A.3. Project participants:****Table 1: Table of project participants**

Name of Party involved	Private and/or public entity (ies) project participants	Kindly indicate if the Party involved wishes to be considered as project participant (Yes/No)
Thailand (host)	Siam Quality Starch Company Limited	No
Japan	Mitsubishi UFJ Securities Co., Ltd.	No

Siam Quality Starch Co., Ltd. (SQS)

SQS is a Thai-based producer of starch since 1995 and is a major producer of tapioca starches in the Asia Pacific, with its products distributed both locally and internationally to destinations including USA, Japan, Europe, Australia and New Zealand. SQS specializes in producing premium quality, food-grade native and modified tapioca starches.

SQS is implementing the project activity.

Mitsubishi UFJ Securities Co., Ltd. (MUS)

Through its Clean Energy Finance Committee, MUS provides consulting services to promote Clean Development Mechanism (CDM) and Joint Implementation (JI) projects. MUS is the CDM advisor to the Project and the contact for the project activity.

A.4. Technical description of the project activity:**A.4.1. Location of the project activity:****A.4.1.1. Host Party(ies):**

Thailand

A.4.1.2. Region/State/Province etc.:

Chaiyaphum Province

A.4.1.3. City/Town/Community etc:

Village 10, Tambol Khokrerngrom, Amphur Bumnetnarong

A.4.1.4. Detail of physical location, including information allowing the unique identification of this project activity (maximum one page):

Chaiyaphum Province is approximately 340 km kilometres north-east of Bangkok and has an area of 12,778 km², sharing borders with the Khon Kaen, Nakhon Ratchasima, Lopburi and Phetchabun

Provinces. The major industry is agriculture, with principal crops including rice, tapioca, sugar cane and some maize.

The factory is located on Route 205 in the South Eastern corner of Chaiyaphum Province, about 10 km West of the nearest township of Kham Ping. The area is completely agricultural, with rice grown in low-lying areas and tapioca or sugar cane grown on higher, dryer ground. Kham Ping consists mainly of a cluster of businesses around an intersection existing to serve the agricultural community plus the Ampher Bumnetnarong Hospital.

The address of the factory is 222 Moo 10, Suranarai Road, Kokroengrom, Bumnet-Narong, Chaiyaphum 36160. The co-ordinates are: longitude 101deg 37min 24.96sec, latitude 15 deg 24min 21.59sec.



Figure 1: Map of Thailand with Chaiyaphum Province highlighted (Courtesy of Wikipedia)

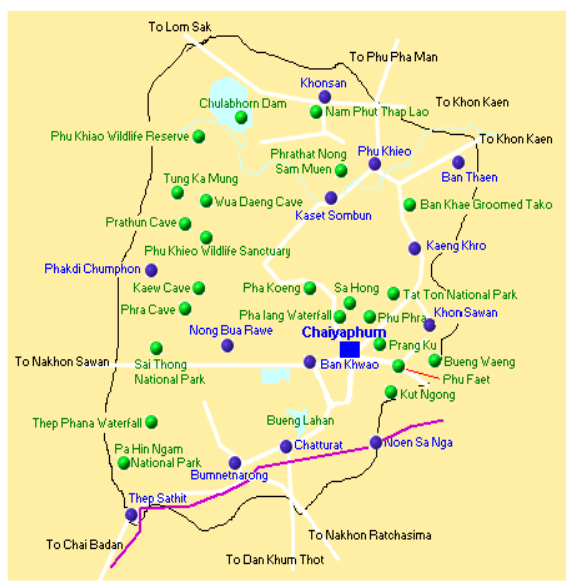


Figure 2: Map of Chaiyaphum Province (Courtesy of sawadee.com)

**A.4.2. Category(ies) of project activity:**

The Project fits under the following two categories of project activity:

- Sectoral Scope 1
Energy industries (renewable / non-renewable sources)
- Sectoral Scope 13
Waste handling and disposal

A.4.3. Technology to be employed by the project activity:**Wastewater treatment system:**

Under the project activity, the wastewater will be treated with a Covered In-Ground Anaerobic Reactor (CIGAR) with a useable volume of 90,000 m³. In the digester, the organic compounds in the wastewater are broken down with the help of anaerobic bacteria, which thrive in the absence of oxygen. The digester is lined with high density polyethylene (HDPE) to prevent both the biogas and wastewater from leaking.

The wastewater is treated in the anaerobic digester for 10 to 15 days, reducing the Chemical Oxygen Demand (COD) load by approximately 80%, and the biogas recovered, before the wastewater is discharged for further treatment in the existing open lagoons.

After lagoon treatment, the final effluent is pumped via underground piping to the surrounding eucalyptus plantation, which covers approximately half of the 120+ hectares of the SQS premises. The method of final discharge remains the same before and after the project activity.

A relatively small amount of sludge is removed infrequently from the existing open lagoons. When sludge is removed, it is either applied to the eucalyptus plantation on-site or given to local farmers for application on tapioca fields as fertilizer.

Energy generation system:

The boilers in the starch plant were originally four thermal oil heaters with a 2 x 3,300kW and 2 x 5,234kW configuration, designed to burn fuel oil. Under the Project, the 2 x 5,234kW burners are retrofitted with “RAY” dual fuel burners such that the boilers can be co-fired using the biogas collected in the CIGAR system. The 2 x 3,300kW burners are completely replaced by new 2 x 5,234kW burners, both in order to allow dual fuel injection and to cater for biogas, which has a low heat content by volume.

Excess biogas flare:

The biogas flare is designed to ignite on overpressure of the biogas supply to the boilers, although it can be operated with a nominal flow to enable a constant flare and reduce the risk of ignition failure. While it has the capacity to handle up to 50% of the biogas flow, under normal operation the flare is not utilized.

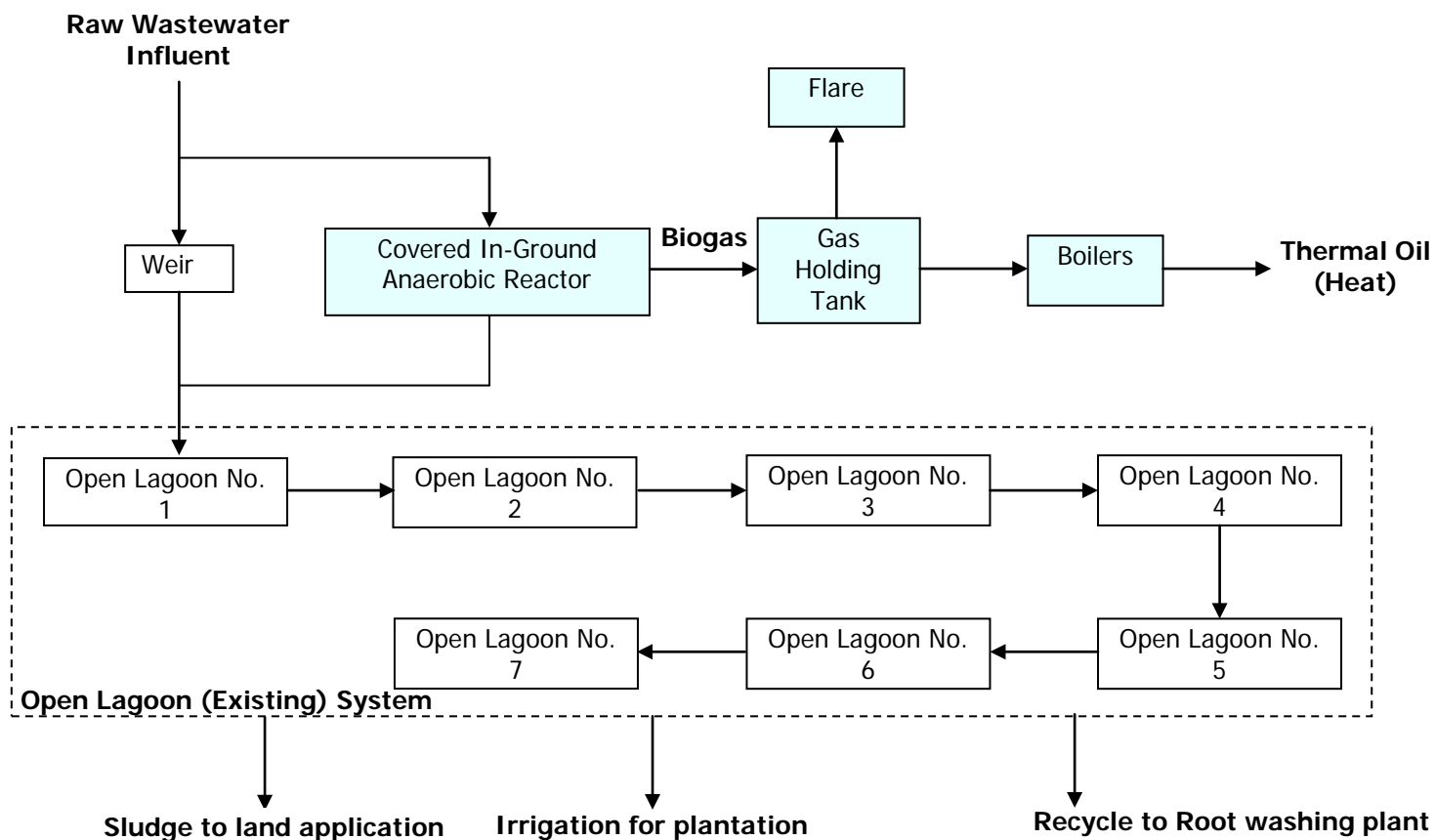


Figure 3: Simple process diagram of Project's wastewater treatment and energy generation systems (additions due to project activity coloured)

A.4.4 Estimated amount of emission reductions over the chosen crediting period:

The estimated amount of emission reductions over the crediting period is shown below.

Table 2: Ex ante estimation of emission reductions

Years	Estimation of annual emission reductions in tonnes of CO ₂ e
2008	98,372
2009	98,372
2010	98,372
2011	98,372
2012	98,372
2013	98,372
2014	98,372
2015	98,372
2016	98,372
2017	98,372
Total estimated reductions (tonnes of CO ₂ e)	983,720



Total number of crediting years	10
Annual average of the estimated reductions over the crediting period (tCO ₂ e)	98,372

A.4.5. Public funding of the project activity:

The Project does not involve funding from an Annex I country.

**SECTION B. Application of a baseline and monitoring methodology****B.1. Title and reference of the approved baseline and monitoring methodology applied to the project activity:**

The following two approved baseline and monitoring methodologies are applied.

- AM0013: “Avoided methane emissions from organic waste-water treatment”
Version 04, valid from 22 December 2006
- AMS-I.C. “Thermal energy for the user”
Version 12, valid from 10 August 2007

For the purpose of establishing additionality, Version 04 of the *Tool for the demonstration and assessment of additionality* (“Additionality Tool”) is also used.

B.2 Justification of the choice of the methodology and why it is applicable to the project activity:

The Project meets all the applicability conditions of the methodologies, as described below.

Table 3: Applicability conditions for AM0013

	Applicability condition	Project case
1	The existing waste water treatment system is an open lagoon system with an ‘active’ anaerobic condition, which is characterized as follows: <ul style="list-style-type: none"> • The depth of the open lagoon system is at least 1m; • The temperature of the anaerobic lagoons is higher than 10°C. If the average monthly temperature in a particular month is less than 10°C, this month is not included in the estimations, as it is assumed that no anaerobic activity occurs below such temperature. • The residence time of the organic matter should be at least 30 days. 	SQS’s wastewater treatment system in the absence of the Project is an actively anaerobic open lagoon system where: <ul style="list-style-type: none"> • The seven open lagoons all have a depth of at least 1m; • The temperature of the anaerobic lagoons is higher than 10°C. The mean temperatures in Chaiyaphum range from 24°C to 30°C¹. • The residence time of the organic matter in open lagoons is approximately 40 to 45 days.
2	Sludge produced during project activity is not stored onsite before land application to avoid any possible methane emissions from anaerobic degradation.	Sludge, which is removed infrequently, is not stored onsite. They are either applied to the eucalyptus plantation or given away to nearby farmers as fertilizer.

Table 4: Applicability conditions for AMS-I.C.

	Applicability condition	Project case
1	This category comprises renewable energy	The project activity involves the supply to users

¹weather.com, accessed March 2007.



	technologies that supply individual households or users with thermal energy that displaces fossil fuels. Examples include solar thermal water heaters and dryers, solar cookers, energy derived from renewable biomass for water heating, space heating, or drying, and other technologies that provide thermal energy that displaces fossil fuel. Biomass-based cogenerating systems that produce heat and electricity for use on-site are included in this category.	of thermal energy derived from renewable biogas that displaces fossil fuels, namely, fuel oil.
2	Where generation capacity is specified by the manufacturer, it shall be less than 15MW.	See 3. below.
3	For co-generation systems and/or co-fired systems to qualify under this category, the energy output shall not exceed 45 MW _{thermal} e.g. for a biomass based co-generating system the capacity for all the boilers affected by the project activity combined shall not exceed 45 MW _{thermal} . In the case of the co-fired system the installed capacity (specified for fossil fuel use) for each boiler affected by the project activity combined shall not exceed 45 MW _{thermal} .	The capacity of the boilers total 17.068MW _{th} and will be co-fired with fuel oil.
4	In the case of project activities that involve the addition of renewable energy units at an existing renewable energy facility, the added capacity of the units added by the project should be lower than 45 MW _{thermal} and should be physically distinct from the existing units.	Not applicable. The project activity does not involve the addition of renewable energy units at an existing renewable energy facility.

B.3. Description of the sources and gases included in the project boundary

As per the methodology, the project boundary includes the existing waste water treatment plant, where sludge is degraded in open sludge lagoons under mainly anaerobic conditions. The following emission sources are included:

Table 5: Sources and gases in the project boundary

	Source	Gas	Included/Excluded	Justification / Explanation
Baseline	Direct emissions from the waste treatment processes	CH ₄	Included	The major source of emissions in the baseline
		N ₂ O	Excluded	Excluded for simplification. This is conservative.
		CO ₂	Excluded	CO ₂ emissions from the decomposition of organic waste are not accounted
	Emissions from electricity consumption / generation	CO ₂	Excluded	Not applicable to the Project.
		CH ₄	Excluded	
		N ₂ O	Excluded	
	Emissions from thermal	CO ₂	Included	Thermal energy generation is



Project activity	energy generation			included in the project activity
		CH ₄	Excluded	Excluded for simplification. This is conservative.
		N ₂ O	Excluded	Excluded for simplification. This is conservative.
	On-site fossil fuel consumption due to the project activity	CO ₂	Included	May be an important emission source
		CH ₄	Excluded	Excluded for simplification. This emission source is assumed to be very small.
		N ₂ O	Excluded	Excluded for simplification. This emission source is assumed to be very small.
	Emissions from on-site electricity use in the digester auxiliary equipment	CO ₂	Included	May be an important emission source. If electricity is generated from collected biogas, these emissions are not accounted for.
		CH ₄	Excluded	Excluded for simplification. This emission source is assumed to be very small.
		N ₂ O	Excluded	Excluded for simplification. This emission source is assumed to be very small.
	Direct emissions from the waste treatment processes	N ₂ O	Excluded	Excluded for simplification. Not an important emission source.
		CO ₂	Excluded	CO ₂ emissions from the decomposition of organic waste are not accounted.
		CH ₄	Included	The emission from uncombusted methane and also leakage in case of anaerobic digesters. In case of dewatering and land application, conservative estimates of methane are included.

B.4. Description of how the baseline scenario is identified and description of the identified baseline scenario:

The most plausible baseline scenario is identified in the following steps:

- Step I. Draw up a list of possible realistic and credible alternatives for the treatment of the sludge;
- Step II. Eliminate alternatives that are not complying with applicable laws and regulations
- Step III. Eliminate alternatives that face prohibitive barriers
- Step IV. Compare economic attractiveness of remaining alternatives

Step I. Draw up a list of possible realistic and credible alternatives for the treatment of the sludge



The alternative scenarios available to SQS and that provide comparable outputs to the Project are summarized in the table below.

Table 6: List of plausible alternatives to the Project

Alternative	Wastewater treatment	Biogas usage	Description of alternative scenario
A	Sequential treatment using CIGAR system and existing open lagoon	Used to produce process heating	The Project undertaken without being registered as a CDM project activity
B	Sequential treatment using CIGAR system and existing open lagoon	Not utilized	The wastewater treatment method is the same as the Project, but does not include biogas utilization and hence smaller capital cost
C	Sequential treatment using anaerobic/aerobic system other than CIGAR and existing open lagoon	Used to produce process heating or not utilized (in the case of aerobic system)	This alternative involves an upgrade to a wastewater treatment system with comparable results to the Project
D	Open lagoons	Uncontrolled release into the atmosphere	This is the continuation of current practice
E	Open lagoons in short- to medium-term, upgrade to sequential treatment using CIGAR system and existing open lagoon in future	Uncontrolled release into the atmosphere in short- to medium-term, used to produce process heating in future	This is the continuation of current practice, with the Project undertaken without being registered as a CDM project activity in the future

Step II. Eliminate alternatives that are not complying with applicable laws and regulations

All alternatives identified are consistent with mandatory laws and regulations.

Step III. Eliminate alternatives that face prohibitive barriers

Of the five alternatives identified in Step I above, all but Alternative D, the continuation of current practice, can be immediately ruled out as plausible alternatives, as delineated below.

Alternative A: As further discussed in Section B.5 below, this alternative involves high risk and upfront capital cost that is not acceptable to SQS in the absence of the CDM.

Alternative B: This is a less advantageous option as compared to Alternative A. While the upfront cost is lower, not only does this alternative involve the same high risks, but there is no cost recovery in the form of reduced fossil fuel consumption.

Alternative C: This is also a less advantageous option as compared to Alternative B. While this alternative provides a comparable output, the CIGAR system utilized in Alternative A is one of the less cost intensive options available for the treatment of wastewater. A more technologically advanced system may provide greater process stability and potentially higher biogas yield, however, the cost was considered too high by SQS to warrant the risky investment.



Alternative D: This is the continuation of current practice. SQS' original plan prior to the decision to proceed with the CDM project activity was to continue treatment of its wastewater in the existing lagoons, and to increase the capacity of the open lagoons either by increasing the number of ponds or increasing the volume of each pond as necessary to cater for any increase in starch production capacity.

Alternative E: This alternative involves the implementation of the Project without the assistance of the CDM not immediately but in the future. For the same reasons outlined for Alternative A, this alternative was not acceptable to SQS. In addition, as briefly discussed in Alternative D, the project circumstances will remain the same in the future, as the SQS starch factory has an abundance of land such that any increase in production capacity or tightening of discharge limits can be catered for by simply increasing the capacity of the open lagoons.

Therefore, the most plausible baseline scenario is Alternative D, the continuation of current practice. This conclusion will be reinforced in the assessment of additionality in the ensuing section.

Step IV. Compare economic attractiveness of remaining alternatives

In this step, it is necessary to compare the economic attractiveness without revenues from CERs for all alternatives that are remaining by applying Step 2 of the latest version of the "Tool for demonstration and assessment of additionality". As identified in Step III above, the only remaining alternative is Alternative D, the continuation of current practice. As the only remaining alternative, an economic comparison is not conducted.

For the economic investment analysis of Alternative A (the CDM project activity), which has already been ruled out, please refer to Section B.5. For clarity, it is noted that the investment analysis in B.5 is separate to the economic analysis referred to here, in Step IV.

B.5. Description of how the anthropogenic emissions of GHG by sources are reduced below those that would have occurred in the absence of the registered CDM project activity (assessment and demonstration of additionality):
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The Project's additionality is demonstrated by applying the latest version of the "Tool for the demonstration and assessment of additionality" (Version 04), which is consistent with Option B of the methodology.

Step 1. Identification of alternatives to the project activity consistent with current laws and regulations

Realistic and credible alternatives to the project activity is identified in this step through the following sub-steps.

Sub-step 1a. Define alternatives to the project activity

See Section B.4. The most plausible baseline scenario is the continuation of current practice.

Sub-step 1b. Consistency with mandatory laws and regulations

All alternatives identified are consistent with mandatory laws and regulations.

**Step 2. Investment analysis**

The IRR is chosen as the most suitable indicator. The Tool allows either the equity or project approaches to be used to calculate the IRR. Here, the equity IRR will be used².

Sub-step 2a – Determine the appropriate analysis method

As the CDM project activity generates financial benefits in the form of reduced consumption of fuel oil, the simple cost analysis is not appropriate. Of the remaining investment comparison analysis and benchmark analysis, the benchmark analysis is chosen.

Sub-step 2b – Option III. Apply benchmark analysis

At the time the Project was being considered by SQS in 2003, the internal benchmark IRR used was 20%, taking into account SQS internal policies and factors such as risk to factory operation. If retrospectively, one applies the benchmark analysis, a premium would have been added to the government bond rate of a little above 4% at the time, to reflect risks to private sector investment and the significant risk inherent to using an unfamiliar technology, particularly in view of the potential to adversely affect the core business at SQS. This would have resulted in a benchmark of between 15% and 20%. A benchmark in this range is supported by the National Energy Policy Office's³ study *Biomass-based Power Generation and Cogeneration within Small Rural Industries of Thailand*, which cites a hurdle rate of 23%. Despite this study being for biomass, rather than biogas fuels, the IRR it cites is pertinent to this Project as the study focuses on energy generation in the context of rural food industries.

For conservatism, an IRR of 15% is adopted.

Sub-step 2c – Calculation and comparison of financial indicators

The following table summarizes the Project's IRR calculation, including all assumptions made.

Table 7: Assumptions and results for calculation of the Project's IRR

Input Parameters		Value	Unit	Notes
Total cost for CDM project activity		75,000,000	THB	
Loan	Equity percentage	100	%	
	Interest rate	N/A		
	Loan period	N/A		
Annual costs	Operation and Maintenance	3,750,000	THB/year	5% of total cost
	Cost of chemicals	5.5	THB/m ³ effluent	To maintain optimal digester operation
Fuel savings		7.77	THB/litre	5-year average oil

² In the Project's case, equity is 100%. Because of this, while the equity approach is chosen for the purpose of the calculation, both equity and project approaches will return the same result.

³ The National Energy Policy Office is the predecessor to the Energy Policy and Planning Office, both under the Ministry of Energy



				price from 1999 – 2003
Depreciation	Depreciation rate	5,769,231	THB/year	
	Salvage value	5,769,231	THB	
Tax rate		30	%	Applied to increased profit from fuel savings
Project life		12	years	
Operating parameters	Operating days in year	330	days	
	COD load of raw effluent	15.0	kg/m ³	Based on historic records
	COD treatment efficiency	80	%	Typical values for type of technology
	Biogas generation rate	0.4	m ³ /kgCOD	
	Biogas methane content	50	% by volume	
	Biogas leakage from digester	15	%	Assumption
	Methane energy content	36.3	MJ/m ³	
	Flare rate	0		For normal operation
Fuel oil heat value	41	MJ/l	From SQS' fuel supplier	
IRR		8.68	%	

As can be seen in the above table, the IRR of the Project if carried out under business-as-usual stands at 8.68%, well below the expected IRR of 15%.

Sub-step 2d – Sensitivity analysis

In order to test the robustness of the assumptions made, sensitivity analyses were carried out as follows:

1. 10% decrease in annual costs (O&M and chemicals). This is a realistic target that SQS is striving to achieve.
2. 20% increase in biogas capture. This is also a target that SQS is striving to achieve, by maximising the quality and stability of the biogas captured.
3. 4% increase in fuel prices. The price rise is based on the average annual price rise over the 5-year period between 1999 and 2003, as calculated in 2003.

The above changes in assumptions increased the IRRs for each of the cases to 10.40%, 14.79% and 14.51% respectively. The sensitivity analyses show that in spite of the range of realistic and optimistic assumptions made, the project returns remain unfavourable.

It is noteworthy that the COD loading of the wastewater is indirectly proportional to the extraction efficiency of the starch in the factory. Thus, maximizing the project activity's returns is at odds with maximizing profits from SQS' core business. Naturally, priority is given to running the core business of starch production, regardless of whether it results a lower COD load and therefore lower biogas yield. The possibility of lower biogas yields exacerbates the problem of a low IRR.



Furthermore, the implementation of the Project required an upgrading of skills for the proper operation and maintenance of the anaerobic digester, as well as the gas burners. There are numerous variables, such as the COD load of incoming wastewater and the temperature conditions that affect the quantity and quality of the biogas. As the quality of the biogas feed is crucial to the smooth operation of the burners, which in turn is important for the uninterrupted operation of the starch factory, the upgrading of skills was a significant challenge to SQS.

The challenge is even more significant when taking into account the context of the food processing industry, where very few plant owners have ventured into advanced technology for wastewater treatment. Indeed, it is understood that most projects which are now attempting to introduce this technology is doing so with the assistance of the CDM, while others did so with funding sources no longer available. Against this backdrop, the technology barrier faced by SQS is too high to justify the risk of going ahead under business-as-usual.

It is noted that with regards to the wastewater treatment system, SQS has abundant land as well as access to cheap land in the vicinity in order to expand its current. The wastewater treatment for the plant expansion could and would have been treated using the existing open lagoon system, either by increasing the number or volume of lagoons. This was what was envisaged when the budget for the plant expansion was originally established in 2003. SQS has access to over 120 ha of available land, more than enough to accommodate such an expansion. It would have been much cheaper to implement this option, as SQS still has available land. It is also noted that the land around the SQS factory was and still is relatively cheap and available for purchase.

Step 4. Common practice analysis

Sub-step 4a – Analyze other activities similar to the proposed project activity

Comparable projects to SQS were identified based on the following characteristics:

1. Appropriate industry.

There are two types of starch, Native and Modified, but only Native starch has wastewater characteristics that will allow biogas recovery from wastewater. Hence, the selection of factories for the common practice analysis excludes Modified starch-only factories.

2. Relevant size.

Starch factories vary significantly in size, and the project circumstances cannot be readily compared between these sizes. What is particularly relevant to additionality assessment is the fact that projects of a large size tend to be more viable than smaller ones due to economy of scale. For this reason, a comparison between the large SQS Project and a wide spectrum of projects could distort the result of common practice analysis to be less conservative than it should be. The selection for the common practice therefore identified plants of a similar scale to SQS.

Two sets of data were used in narrowing down the factories. These are:

- a. A list obtained from the Thai Tapioca Starch Association, which lists the starch plants and technologies employed for wastewater treatment. This list was compiled in April 2007 based on a survey TTSA sent out to the factories. As stated in 1 above, Modified starch-only factories were excluded.



- b. A list obtained from the Department of Industrial Works which lists, among others, the size of the factory in terms of horsepower which will be a reasonable indicator of starch production capacity. The DIW list gives the SQS factory's horsepower as 14,773. For the purpose of narrowing down the comparable projects based on criteria 2 stated above, the list was narrowed down to factories that were of similar size as SQS or larger.

Originals of both lists have been submitted to the DOE.

To summarize the result of the common practice assessment, it was found that there were four factories that should be compared against the Project, as listed below. Three of the four factories used comparable technologies to the Project, while another did not have a biogas recovery technology. Consistent with the "Tool for the demonstration and assessment of additionality", none of the three factories were considered similar as all were/are carried out with the assistance of carbon credits, one as a registered CDM project, and others at various stages of the CDM process. It was thus concluded that the Project is not a common practice.

Table 8: List of comparable factories in order of decreasing size (horsepower)

Company	Size (horsepower)	Biogas system	Notes
Sanguan Wongse Industry Co., Ltd.	30,505	Yes	Registered CDM project (Project 1040)
Eiamheng Tapioca Flour Industry Co., Ltd.	21,130	Yes	Applying for CDM ⁴
Eiamburapa Co., Ltd.	15,821	Yes	Applying for CDM ⁵
Siam Quality Starch Co., Ltd.	14,773	Yes	The project activity
Sangpetch Tapioca Flour Co., Ltd.	13,084	No	N/A

Sub-step 4b – Discuss any similar options that are occurring

No similar options are occurring.

Starting dates of the project activity and validation

Consistent with EB41 Annex 46 "Guidance on the demonstration and assessment of prior consideration of the CDM" it is required that where the starting date of the project activity falls before 2 August 2008, evidence is to be provided to show that (a) the project participant had awareness of the CDM prior to the project activity start date, and that the benefits of the CDM were a decisive factor in the decision to proceed with the project, and (b) continuing and real actions were taken to secure CDM status for the project in parallel with its implementation. As given in Section C.1.1., the starting date of the project activity, here defined as the date on which the pond linings were ordered, was 31 March 2005, which is prior to 2 August 2008.

There is ample evidence to show that SQS seriously considered the CDM from the very early stages of the project development. The Project was considered only after it became known that the Korat

⁴http://www.tgo.or.th/index.php?option=com_content&task=view&id=37&itemid=29&task=view&id=37&itemid=29

⁵<http://cdm.unfccc.int/Projects/Validation/DB/A8JT0K03JKGLSDSV1O1Y0JISTYYNHN/view.html>



wastewater project, the first wastewater-related project in Thailand, had started developing its project as a CDM. Various consultants emphasized the attractiveness of such a project due to the CER revenues, and there was much talk in the industry from all biogas digester suppliers. It is also worth noting that in 2003, SQS' joint venture partner of the time, AVEBE BA of The Netherlands, strongly recommended to proceed with the Project, which however was rejected by SQS management. It was only after the submission of a proposal by Waste Solutions, the same consultant to the Korat project, which had incorporated the CDM into its plans, that SQS made the decision to proceed. The said meeting minutes and proposal have been provided as evidence to the DOE during the course of the validation.

It is pertinent to note that despite pioneering efforts by Thai developers, who were among the first in the world to attempt to develop CDM projects from as early as 2001, the first batch of LoAs were not handed out until 2007. Because of this delay, many early Thai developers adopted an active approach to lobby the Thai government, whilst others including SQS adopted a wait-and-see approach, and kick-started the formal CDM process as soon as there were real signs of DNA approval⁶. However, SQS was unable to obtain the LoA earlier, due to a new DNA rule introduced immediately after the first batch of retroactive projects were approved, which required all projects applying for the CDM to first submit an Initial Environment Evaluation Report, a report for which SQS had to retain a licensed consultant to work on the project for several months and which set back the overall CDM process for many more months.

A complete timeline, including a list of submitted evidence, is summarized in the below table.

Table 9: Complete timeline

Date	Action	Relevance to paragraph 5	Note
07/10/2003	SQS agrees with joint venture partner to conduct pilot study for biogas system.	<i>Awareness of the CDM prior to the project activity start date</i>	Excerpt of Avebe visit report submitted.
19/09/2004	SQS concludes after pilot study that the biogas system is not viable without carbon credits.		SQS internal email to senior management submitted.
14/05/2004	SQS visits Sanguan Wongse factory (host factory of Korat Waste to Energy Project, project 1040)		
29/10/2004	SQS receives proposal for engineering services from Waste Solutions, which explicitly includes CDM revenue.	<i>Awareness of the CDM prior to the project activity start date; The benefits of the CDM were a decisive factor in the decision to proceed with the project</i>	Excerpt of the proposal submitted.
20/01/2005	SQS executes contract with Waste Solutions for engineering services.	<i>The benefits of the CDM were a decisive factor in the decision to proceed with the</i>	Excerpt of contract submitted.

⁶ At the time, MUS, SQS' CDM consultant, which is also CDM consultant to A.T. Biopower (project 1026), had intimate knowledge of the progress of the DNA approvals, including the request to the CDM Executive Board led by A.T. Biopower for a special extension of the deadline for retroactive credits.



		<i>project</i>	
31/03/2005	Project start date as per Section C.1.1. (ordered linings for the CIGAR system)		As confirmed in Validation Report p37.
20/12/2005	SQS initiates discussion with MUS (CDM consultant to the Project).	<i>Continuing and real actions were taken to secure CDM status for the project in parallel with its implementation</i>	Email from SQS submitted.
24/03/2006	SQS receives formal CDM consultancy proposal from MUS after extensive discussions.		Excerpt of proposal submitted.
31/03/2006	SQS accepts MUS proposal		Email between SQS and MUS submitted.
18/04/2006	Negotiations with MUS begin in earnest		Emails between SQS and MUS, dated April 2, April 3, April 18, May 4, May 19, and June 23 submitted.
13/10/2006	Email sent by MUS to UNFCCC on behalf of early start Thai projects for the extension of deadline for retroactive projects.	N/A – shows delay in Thai project approval process	Email submitted.
22/11/2006 (principal agreement) and 29/12/2006 (minor correction)	CDM consultancy agreement between SQS and MUS executed after 8 months' negotiations through lawyers on both sides.	<i>Continuing and real actions were taken to secure CDM status for the project in parallel with its implementation</i>	Emails between SQS and MUS, dated November 3 ⁷ , 15, 22, 30, December 18, 19, 21 and 29 submitted. It is noted that SQS hired an external lawyer at considerable expense to negotiate the agreement, which is a CDM transaction cost.
30/01/2007	Thai cabinet approves first batch of projects after years of lobbying by a handful of pioneering project developers	N/A – shows delay in Thai project approval process	Public knowledge. Point Carbon article submitted.
08/03/2007 – 08/06/2008	MUS enquires with ONEP regarding the new approval process	<i>Continuing and real actions were taken to secure CDM status for the project in parallel with its implementation</i>	Email submitted. It is noted that around this time, ONEP introduced a new requirement for an

⁷ It is noted that there were extensive communications between SQS and MUS between June 23 and November 3, however these were not submitted to the DOE as they contain commercially sensitive information relating to the contract negotiations carried out by lawyers on both sides.



			Initial Environmental Evaluation to be carried out for the sake of host country approval, even if it were not required by any other regulation. The eventual confirmation came on June 08, 2007. SQS was subsequently notified of this new requirement.
06/07/2007	Thailand Greenhouse Gas Management Organization (TGO) established with a view to taking over approval process from cabinet	N/A – shows delay in Thai project approval process	Public knowledge.
11/07/2007 & 01/08 /2007	SQS receives quotes for IEE in response to new rules	<i>Continuing and real actions were taken to secure CDM status for the project in parallel with its implementation</i>	Formal proposal dated August 1 submitted. It is noted it took several months to obtain the quote as there was confusion as to whether an ONEP-registered IEE consultant was required ⁸ .
28/08/2007	Thai cabinet approves second batch of projects which missed out in the first round	N/A – shows delay in Thai project approval process	Public knowledge. Point Carbon article submitted.
14/09/2007	SQS contracts IEE consultant	<i>Continuing and real actions were taken to secure CDM status for the project in parallel with its implementation</i>	Contract submitted.
26/07/2007	MUS requests SGS proposal for Validation		In DOE archive.
26/09/2007	PDD uploaded to UNFCCC website		Public knowledge.
28/09/2007	Validation site visit by DOE		As per Validation Report.
06/03/2008	IEE completed		
07/03/2008	Request for Thai DNA approval		PDD submitted together with completed IEE.
24/03/2008	Request for Japanese DNA approval		
10/06/2008	Japanese DNA approval		Refer to LoA.
14/07/2008	Thai DNA approval		Refer to LoA.

⁸ It was eventually clarified with TGO that a registered consultant was not required, however this was after SQS retained a registered consultant.



			It is noted that this approval was obtained at record speed at the time, as a result of intense lobbying with the TGO, who was sympathetic to SQS' plight. Had the approval not been achieved in time, the grace period on the methodology would have lapsed, further delaying CDM progress.
04/08/2008	Final Validation Report issued by DOE		In DOE archive.
05/08/2008	Request for Registration		In DOE archive.

In summary, there can be no doubt that the SQS Project meets the requirements of paragraph 5, Annex 46, EB41.

B.6. Emission reductions:

B.6.1. Explanation of methodological choices:

The emission reductions due to the Project is calculated in the following manner.

$$ER_y = BE_y - PE_y \quad \text{Equation 1}$$

where

$$BE_y = BE_{\text{lagoon},y} + BE_{\text{fuel_oil},y} \quad \text{Equation 2}$$

and

$$PE_y = PE_{\text{lagoon},y} + PE_{\text{phys_leak},y} + PE_{\text{sludge},y} + PE_{\text{dewater},y} + PE_{\text{energy_cons},y} + PE_{\text{stack},y} \quad \text{Equation 3}$$

where

- $BE_{\text{lagoon},y}$ = Baseline CH₄ emissions from the open lagoons in year y (tCO₂e/yr)
- $BE_{\text{fuel_oil},y}$ = Baseline CO₂ emissions from the combustion of fuel oil in year y (tCO₂/yr)
- $PE_{\text{lagoon},y}$ = Project CH₄ emissions from the open lagoons in year y (tCO₂e/yr)
- $PE_{\text{phys_leak},y}$ = Project CH₄ emissions due to the physical leakage from the anaerobic digester in year y (tCO₂e/yr)
- $PE_{\text{sludge},y}$ = Project CH₄ emissions from the land application of sludge in year y (tCO₂e/yr)
- $PE_{\text{dewater},y}$ = Project CH₄ emissions from wastewater removed in the dewatering process in year y (tCO₂e/yr)
- $PE_{\text{energy_cons},y}$ = Project CO₂ emissions from the consumption of energy on the account of the project activity in year y (tCO₂/yr)
- $PE_{\text{stack},y}$ = Project CH₄ emissions from incomplete combustion of biogas in the flare and boilers in year y (tCO₂e/yr)



In the Project's case, $PE_{\text{dewater},y}$ is not relevant and so Equation 3 becomes:

$$PE_y = PE_{\text{lagoon},y} + PE_{\text{phys_leak},y} + PE_{\text{sludge},y} + PE_{\text{energy_cons},y} + PE_{\text{stack},y}$$

No leakage is associated with the project activity.

The calculation method and input values of the baseline and project emissions are described in the ensuing tables.

Table 10: Formulae, input values and data sources for the calculation of $BE_{\text{lagoon},y}$

Parameter	Description	Value	Source
$BE_{\text{lagoon},y} = \sum_m (\text{COD}_{\text{available},m} \times \text{MCF}_{\text{baseline},m}) \times B_o \times \text{GWP}_{\text{CH}_4}$			Equation 4
$\text{COD}_{\text{available},m}$	Monthly COD available for conversion which is equal to sum of the monthly COD entering the digester ($\text{COD}_{\text{baseline},m}$) and the COD carried over from the previous month (kgCOD)	Calculated	Refer to Equation 5
$\text{MCF}_{\text{baseline},m}$	Monthly methane conversion factor for the open lagoons in the baseline case (fraction)	Calculated	Refer to Equation 8
B_o	Maximum methane producing capacity (kgCH ₄ /kgCOD)	0.21	AM0013
GWP_{CH_4}	Global warming potential for methane (tCO ₂ e/tCH ₄)	21	AM0013, consistent with IPCC
$\text{COD}_{\text{available},m} = \text{COD}_{\text{baseline},m} + \text{COD}_{\text{carryover},m-1}$			Equation 5
$\text{COD}_{\text{baseline},m}$	Monthly COD of effluent entering lagoons (kgCOD)	Calculated	Refer to Equation 6
$\text{COD}_{\text{carryover},m-1}$	COD that remains in the system from the previous month (kgCOD)	Calculated	Refer to Equation 7
$\text{COD}_{\text{baseline},m} = \text{COD}_{\text{conc_in,baseline},m} \times \left(1 - \frac{\text{COD}_{\text{conc_out,baseline},m}}{\text{COD}_{\text{conc_in,baseline},m}} \right) \times F_{\text{digester}} \times \text{OP}_m$			Equation 6
			N/A
$\text{COD}_{\text{conc_in,baseline},m}$	COD concentration of effluent entering the lagoons in the baseline (kgCOD/m ³)	15	SQS, to be monitored
$\text{COD}_{\text{conc_out,baseline},m}$	COD concentration of final effluent in the baseline (kgCOD/m ³)	0.12	Maximum allowable level under government regulations



F_{digester}	Flow rate of wastewater fed in to the digester (m^3/day)	6,000		SQS, to be monitored. Total maximum raw effluent from the factory is $7,200\text{m}^3/\text{day}$.
OP_m	Number of operation days in month (day)	Month	Op. Day	SQS, to be monitored
		Jan	31	
		Feb	28	
		Mar	31	
		Apr	30	
		May	31	
		Jun	30	
		Jul	-	
		Aug	31	
		Sep	30	
		Oct	31	
		Nov	30	
Dec	31			
Equation 7				
$COD_{\text{carryover},m-1} = \left[COD_{\text{available},m-1} \times (1 - MCF_{\text{baseline},m-1}) \right] - (Q_{\text{sludge},m-1} \times COD_{\text{conc_sludge},m-1})$				
$COD_{\text{available},m-1}$	COD available in previous month (kgCOD)	Calculated	As per calculation of COD available,m	
$MCF_{\text{baseline},m-1}$	Monthly methane conversion factor for the open lagoons in the baseline case in previous month (fraction)	Calculated	Refer to Equation 8	
$Q_{\text{sludge},m-1}$	Amount of sludge removed in previous month (m^3)	100% of carryover removed annually	SQS, to be monitored. Sludge is currently removed less than once a year	
$COD_{\text{conc_sludge},m-1}$	COD concentration of sludge removed in previous month (kgCOD/ m^3)			
Equation 8				
$MCF_{\text{baseline},m} = f_d \times f_{t,m} \times 0.89$				
f_d	Fraction of anaerobic degradation as a function of depth (fraction)	0.7 (>5m) 0.5 (1 – 5m) 0 (<1m)	AM0013	
$f_{t,m}$	Fraction of anaerobic degradation as a function of temperature, on a monthly basis, where $f_{t,m} \leq 1$ (fraction)	Calculated	Refer to Equation 9	
Equation 9				
$f_{t,m} = \exp\left(\frac{E \times (T_2 - T_1)}{R \times T_1 \times T_2}\right)$				
E	Activation energy constant (cal/mol)	15,175	Constant	
T_2	Ambient temperature ($^{\circ}\text{K}$)	Month	Temp	Based on ambient



		Jan	297.16	temperature records, to be monitored
		Feb	300.16	
		Mar	302.16	
		Apr	303.16	
		Ma	302.16	
		y		
		Jun	301.16	
		Jul	301.16	
		Aug	301.16	
		Sep	300.16	
		Oct	300.16	
		Nov	299.16	
		Dec	297.16	
T_1	Reference temperature (°K)		303.16	Constant
R	Ideal gas constant (cal/kmol)		1,987	Constant

Table 11: Formula, input values and data sources for the calculation of $BE_{fuel_oil,y}$

Parameter	Description	Value	Source
Equation 10			
$BE_{fuel_oil,y} = Q_{fuel_oil,y} \times CO_2EF_{fuel} \times OX_{fuel}$			
$Q_{fuel_oil,y}$	Quantity of fuel oil consumed in year y at the project site in the absence of the project activity (TJ)	140.6	SQS, 3 year historical records. Actual displacement to be calculated <i>ex post</i> based on the monitored amount of biogas used in the Project. In accordance with AM0013, emission reduction claims for this activity will be capped at 140.6TJ.
CO_2EF_{fuel}	CO_2 emission factor for thermal energy generation using fuel oil (t CO_2 /TJ)	77.4	IPCC 2006 Table 2.2
OX_{fuel}	Oxidation factor for fuel oil (fraction)	1	IPCC 2006 Table 1.4

Table 12: Formula, input values and data sources for the calculation of $PE_{lagoon,y}$

Parameter	Description	Value	Source
Equation 11			
$PE_{lagoon,y} = \sum_m (F_{dig_out,m} \times COD_{conc_dig_out,m} \times OP_m \times MCF_{project,m}) \times B_o \times GWP_{CH_4}$			
$F_{dig_out,m}$	Flow rate of wastewater in exiting the digester to enter the open lagoons in the project activity (m ³ /day)	6,000	SQS, to be monitored
$COD_{conc_dig_out,m}$	Monthly COD of wastewater exiting	3.0	SQS, to be



	the digester to enter the open lagoons in the project activity (kgCOD/m ³)		monitored
OP _m	See above	See above	See above
MCF _{project,m}	Monthly methane conversion factor for the open lagoons in the project case (fraction)	Calculated	Calculated as per Equation 8, where MCF _{project,m} is analogous to MCF _{baseline,m}
B _o	As per Table 8	See above	See above
GWP _{CH₄}	As per Table 8	See above	See above

Table 13: Formula, input values and data sources for the calculation of PE_{phys_leak,y}

Parameter	Description	Value	Source
$PE_{phys_leak,y} = Q_{biogas_total,y} \times W_{CH_4} \times \rho_{CH_4} \times LF \times GWP_{CH_4}$			Equation 12
Q _{biogas_total,y}	Quantity of biogas produced and collected in the digester in year y (m ³ biogas/yr)	8,078,400	SQS, to be monitored
W _{CH₄}	Fraction of CH ₄ in biogas (m ³ CH ₄ /m ³ biogas)	0.5	SQS, to be monitored
ρ _{CH₄}	Density of CH ₄ (tCH ₄ /m ³ CH ₄)	0.00065	Approximate for 30°C based on density of 0.0007168 tCH ₄ /m ³ CH ₄ at STP
LF	Rate of physical leakage from digester (fraction)	0.15	Default value provided in AM0013, to be monitored if lower value applied
GWP _{CH₄}	As per Table 8	See above	See above

Table 14: Formula, input values and data sources for the calculation of PE_{sludge,y}

Parameter	Description	Value	Source
$PE_{sludge,y} = Q_{sludge,y} \times (COD_{sludge,y} \times B_o \times MCF_{la} \times GWP_{CH_4} + NC \times EF_{N_2O} \times GWP_{N_2O})$			Equation 13
Q _{sludge,y}	Quantity of sludge generated by the wastewater treatment in year y (t)	324	SQS, to be monitored
COD _{sludge,y}	Chemical Oxygen Demand of the sludge used for land application (kgCOD/kg sludge)	0.10	Assumed in absence of <i>ex ante</i> data, to be monitored
B _o	See above	See above	See above
MCF _{la}	Methane correction factor of the sludge in year y (fraction)	0.05	AM0013



GWP _ CH ₄	See above	See above	See above
NC	Nitrogen content of sludge (kgN/kg sludge)	0.10	Assumed in absence of <i>ex ante</i> data, to be monitored
EF _{N₂O}	Emission factor of nitrogen from sludge applied to land (kgN ₂ O/kgN)	0.016	AM0013
GWP _ N ₂ O	Global warming potential for nitrous oxide (tCO ₂ e/tN ₂ O)	310	IPCC

Table 15: Formula, input values and data sources for the calculation of PE_{energy_cons,y}

Parameter	Description	Value	Source
Equation 14			
$PE_{energy_cons,y} = Q_{elec_cons,y} \times CO_2EF_{elec} + Q_{fuel_cons,y} \times CO_2EF_{fuel} \times OX_{fuel}$			
$Q_{elec_cons,y}$	Quantity of electricity consumed due to the project activity in year y (MWh)	0	SQS, to be monitored
CO_2EF_{elec}	CO ₂ emissions factor for electricity consumed at the project site (tCO ₂ /MWh)	N/A	Calculated as per AMS-I.D., in the case electricity is consumed
$Q_{fuel_cons,y}$	Quantity of fuel oil consumed due to the project activity in year y (TJ)	0	SQS, to be monitored
CO_2EF_{fuel}	As per Table 9	As above	As above
OX_{fuel}	As per Table 9	As above	As above

Table 16: Formula, input values and data sources for the calculation of PE_{stack,y}

Parameter	Description	Value	Source
Equation 15			
$PE_{stack,y} = [Q_{biogas_burner,y} \times (1 - CE_{burner}) + Q_{flare,y} \times (1 - CE_{flare})] \times W_{CH_4} \times \rho_{CH_4} \times GWP_{CH_4}$			
$Q_{biogas_burner,y}$	Quantity of biogas to be fed to burner in year y (m ³ biogas/year)	8,078,400	SQS, to be monitored
CE_{burner}	Combustion efficiency of burner (fraction)	0.995	SQS, to be monitored
$Q_{flare,y}$	Quantity of biogas to be fed to flare in year y (m ³ biogas/year)	0	SQS, to be monitored
CE_{flare}	Combustion efficiency of flare (fraction)	0.5	Default value provided in Flaring Tool, for open flare. To be monitored
W_{CH_4}	As per Table 11	As above	As above
ρ_{CH_4}	As per Table 11	As above	As above
GWP _ CH ₄	As per Table 8	As above	As above

B.6.2. Data and parameters that are available at validation:



Data / Parameter:	$\text{COC}_{\text{conc_out,baseline,m}}$
Data unit:	kgCOD/m^3
Description:	COD concentration of final effluent in the baseline
Source of data used:	Thai government regulation
Value applied:	0.12
Justification of the choice of data or description of measurement methods and procedures actually applied :	Although the actual discharge load may be lower, the maximum allowable COD load under government regulations, 0.12 kgCOD/m^3 , is used for simplicity and conservatism.
Any comment:	N/A

Data / Parameter:	f_d
Data unit:	Fraction
Description:	Fraction of anaerobic degradation as a function of depth
Source of data used:	AM0013
Value applied:	0.5
Justification of the choice of data or description of measurement methods and procedures actually applied :	This is set as a function of lagoon depth, as per AM0013.
Any comment:	N/A

B.6.3 Ex-ante calculation of emission reductions:

B.6.3.1 Baseline emissions

Estimation of $\text{BE}_{\text{lagoon,y}}$

The formulae and input values given in Table 8 were used to calculate $\text{BE}_{\text{lagoon,y}}$. The results are summarized in Table 15.

Table 17: $\text{BE}_{\text{lagoon,y}}$ for year

Month	Average Ambient Temperature (°C)	$f_{t,m}$	$\text{MCF}_{\text{baseline,m}}$	$\text{COD}_{\text{available,m}}$	$\text{BE}_{\text{lagoon,y}}$
January	24	0.60	0.27	2,767,680	3,266
February	27	0.78	0.35	4,526,941	6,906
March	29	0.92	0.41	5,728,531	10,343
April	30	1.00	0.45	6,061,649	11,896
May	29	0.92	0.41	6,131,895	11,071
June	28	0.85	0.38	6,299,874	10,459



July	28	0.85	0.38	3,928,308	6,521
August	28	0.85	0.38	5,217,190	8,661
September	27	0.78	0.35	5,931,597	9,049
October	27	0.78	0.35	6,647,249	10,141
November	26	0.71	0.32	7,026,041	9,845
December	24	0.60	0.27	7,561,251	8,923
Total for year					107,081

Estimation of $BE_{fuel_oil,y}$

Using the formula and input values given in Table 9, $BE_{fuel_oil,y}$ was calculated as 10,882 tCO₂/yr.

B.6.3.2 Project emissions**Estimation of $PE_{lagoon,y}$**

Based on the formula and input values provided in Table 10, $PE_{lagoon,y}$ was calculated as 9,415tCO₂e/yr.

Estimation of $PE_{phys_leak,y}$

Using the formula and input values given in Table 11, $PE_{phys_leak,y}$ was calculated as 9,730tCO₂e/yr.

Estimation of $PE_{sludge,y}$

$PE_{sludge,y}$ was calculated based on the formula and input values provided in Table 12. The emissions from this source was estimated as 170tCO₂e/yr.

Estimation of $PE_{energy_cons,y}$

The emissions from this source was not estimated ex ante, as the increased consumption of grid electricity or fossil fuel on the account of the CDM project activity was considered minimal. Nevertheless, this will be monitored.

Estimation of $PE_{stack,y}$

Based on the formula and input values provided in Table 14, $PE_{stack,y}$ was calculated as 276tCO₂e/yr.

B.6.4 Summary of the ex-ante estimation of emission reductions:**Table 18: Ex-ante estimation of emission reductions**

Year	Estimation of project activity emissions (tCO ₂ e)	Estimation of baseline emissions (tCO ₂ e)	Estimation of leakage (tCO ₂ e)	Estimation of overall emission reductions (tCO ₂ e)
------	---	---	--	--



2008	19,591	117,963	0	98,372
2009	19,591	117,963	0	98,372
2010	19,591	117,963	0	98,372
2011	19,591	117,963	0	98,372
2012	19,591	117,963	0	98,372
2013	19,591	117,963	0	98,372
2014	19,591	117,963	0	98,372
2015	19,591	117,963	0	98,372
2016	19,591	117,963	0	98,372
2017	19,591	117,963	0	98,372
Total (tonnes of CO ₂ e)	195,910	1,179,630	0	983,720

B.7 Application of the monitoring methodology and description of the monitoring plan:
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B.7.1 Data and parameters monitored:

Data / Parameter:	$F_{\text{digester}} / F_{\text{dig_out,m}}$
Data unit:	m ³ /hr
Description:	Flow rate of wastewater fed in to / discharge out of the digester
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.5	6,000
Description of measurement methods and procedures to be applied:	The flow rate is measured continuously using a flow meter. As the digester is kept in hydraulic balance, only one monitoring point is necessary.
QA/QC procedures to be applied:	The flow meter will be calibrated according to appropriate industry/international standards. The product of the measured flow rate and the measured COD load can be double checked against the factory's starch production records, with which there is a direct correlation.
Any comment:	Used for the calculations of $BE_{\text{lagoon,y}}$ and $PE_{\text{lagoon,y}}$

Data / Parameter:	OP_m								
Data unit:	Day								
Description:	Number of operation days in month								
Source of data to be used:	SQS								
Value of data applied for the purpose of calculating expected emission reductions in section B.5	<table border="1"> <thead> <tr> <th>Month</th> <th>Operating Days</th> </tr> </thead> <tbody> <tr> <td>January</td> <td>31</td> </tr> <tr> <td>February</td> <td>28</td> </tr> <tr> <td>March</td> <td>31</td> </tr> </tbody> </table>	Month	Operating Days	January	31	February	28	March	31
Month	Operating Days								
January	31								
February	28								
March	31								



	April	30
	May	31
	June	30
	July	-
	August	31
	September	30
	October	31
	November	30
	December	31
	Description of measurement methods and procedures to be applied:	Based on biodigester operation
QA/QC procedures to be applied:	N/A	
Any comment:	Used for the calculation of $BE_{lagoon,y}$	

Data / Parameter:	$COD_{conc_in,baseline,m}$
Data unit:	kgCOD/m ³
Description:	COD concentration of effluent entering the lagoons in the baseline
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.5	15
Description of measurement methods and procedures to be applied:	This is equivalent to the COD concentration of raw effluent from the starch factory. The COD load will be measured either using standard COD tests either in house or through an outside laboratory, typically once a day.
QA/QC procedures to be applied:	Standard calibration will be carried out.
Any comment:	Used for the calculation of $BE_{lagoon,y}$

Data / Parameter:	T_2											
Data unit:	°K											
Description:	Ambient temperature											
Source of data to be used:	SQS, directly measured											
Value of data applied for the purpose of calculating expected emission reductions in section B.5	<table border="1"> <thead> <tr> <th rowspan="2">Month</th> <th colspan="2">Average Ambient Temperature</th> </tr> <tr> <th>(°C)</th> <th>(°K)</th> </tr> </thead> <tbody> <tr> <td>January</td> <td>24</td> <td>297.16</td> </tr> <tr> <td>February</td> <td>27</td> <td>300.16</td> </tr> </tbody> </table>	Month	Average Ambient Temperature		(°C)	(°K)	January	24	297.16	February	27	300.16
Month	Average Ambient Temperature											
	(°C)	(°K)										
January	24	297.16										
February	27	300.16										



	March	29	302.16	
	April	30	303.16	
	May	29	302.16	
	June	28	301.16	
	July	28	301.16	
	August	28	301.16	
	September	27	300.16	
	October	27	300.16	
	November	26	299.16	
	December	24	297.16	
Description of measurement methods and procedures to be applied:	Daily average will be monitored, and translated to monthly average.			
QA/QC procedures to be applied:	The results will be checked against local weather data from an official source.			
Any comment:	Used for the calculation of $BE_{\text{lagoon},y}$			

Data / Parameter:	$D_{\text{lagoon,project}}$ (for every pond)
Data unit:	M
Description:	Depth of open lagoons
Source of data to be used:	SQS
Value of data applied for the purpose of calculating expected emission reductions in section B.5	4.5m for all ponds
Description of measurement methods and procedures to be applied:	A marker will be put in place that will indicate the 5m depth, and daily checks will be conducted to show whether the depth is below or above this height.
QA/QC procedures to be applied:	N/A
Any comment:	Used for the calculation of $BE_{\text{lagoon},y}$

Data / Parameter:	$Q_{\text{sludge},m} / Q_{\text{sludge},y}$
Data unit:	m^3 / yr or t / yr
Description:	Amount of sludge generated and removed in month / year
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in	For the purpose of estimating $BE_{\text{lagoon},y}$, removal of 100% sludge at year end was assumed. In practice, sludge removal only occurs very infrequently. For estimating $PE_{\text{sludge},y}$, a figure of 324 t/yr was used, based on extrapolation of



section B.5	operating parameters.
Description of measurement methods and procedures to be applied:	The quantity of sludge will be either weighed or measured with a flow meter or V-notch weir and measurement of solids content.
QA/QC procedures to be applied:	Weight scales and flow and density meters will be calibrated according to relevant industry/international standards.
Any comment:	Used for the calculation of $BE_{lagoon,y}$ and $PE_{sludge,y}$

Data / Parameter:	$COD_{conc_sludge,m}$
Data unit:	$kgCOD/m^3$
Description:	COD concentration of sludge removed in month
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.5	N/A. In <i>ex ante</i> estimation it is assumed sludge is carried over until year end, when all sludge is removed.
Description of measurement methods and procedures to be applied:	The COD load will be measured either using standard COD tests either in house or through an outside laboratory. As sludge is removed infrequently, less than once a year, the COD test will be carried out not at any set interval, but as sludge removal occurs.
QA/QC procedures to be applied:	Standard calibration will be carried out.
Any comment:	Used for the calculation of $BE_{lagoon,y}$

Data / Parameter:	$Q_{fuel_oil,y}$
Data unit:	TJ
Description:	Quantity of fuel oil displaced in year y
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.5	140.6
Description of measurement methods and procedures to be applied:	The quantity of thermal energy displaced is equivalent to the energy content of the biogas fed into the burners for production of hot oil.
QA/QC procedures to be applied:	The meter will be calibrated according to appropriate industry/international standards.
Any comment:	Used for the calculation of $BE_{fuel_oil,y}$. As per AM0013, this value is to be capped at 140.6TJ which is the average of three years' historical consumption.



Data / Parameter:	$COD_{conc_dig_out,m}$
Data unit:	kgCOD/m ³
Description:	COD out of biodigester to lagoons
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.5	3
Description of measurement methods and procedures to be applied:	The COD load will be measured using standard COD tests either in house or through an outside laboratory, typically once a day.
QA/QC procedures to be applied:	Standard calibration will be carried out.
Any comment:	Used for the calculation of $PE_{lagoon,y}$

Data / Parameter:	$Q_{biogas_total,y}$
Data unit:	m ³ /yr
Description:	Quantity of biogas produced and collected in the digester in year y
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.5	8,078,400
Description of measurement methods and procedures to be applied:	Flow meters are used to measure the quantity of biogas collected on a continuous basis, and data aggregated annually.
QA/QC procedures to be applied:	The flow meters will be calibrated according to appropriate industry/international standards.
Any comment:	Used for the calculation of $PE_{phys_leak,y}$

Data / Parameter:	W_{CH_4}
Data unit:	m ³ CH ₄ /m ³ biogas (wet basis)
Description:	Fraction of methane in biogas
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.5	0.5



Description of measurement methods and procedures to be applied:	The methane content in biogas will be monitored using online measurements.
QA/QC procedures to be applied:	The gas analyzer will be calibrated according to appropriate industry/international standards.
Any comment:	Used for the calculation of $PE_{phys_leak,y}$ and $PE_{stack,y}$

Data / Parameter:	$COD_{sludge,y}$
Data unit:	kgCOD/m ³ sludge or kgCOD/t sludge
Description:	Chemical Oxygen Demand of the sludge used for land application
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.5	0.10
Description of measurement methods and procedures to be applied:	At least monthly, or as sludge removal occurs, if sludge removal occurs less frequently.
QA/QC procedures to be applied:	Standard calibration will be carried out.
Any comment:	For the calculation of $PE_{sludge,y}$

Data / Parameter:	NC
Data unit:	kgN/kg sludge
Description:	Nitrogen content of sludge
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.5	0.10
Description of measurement methods and procedures to be applied:	At least monthly, or as sludge removal occurs, if sludge removal occurs less frequently.
QA/QC procedures to be applied:	Standard calibration will be carried out.
Any comment:	For the calculation of $PE_{sludge,y}$

Data / Parameter:	$Q_{elec_cons,y} / Q_{elec_cons,y}$
Data unit:	MWh / TJ



Description:	Quantity of electricity / fuel oil consumed due to the project activity in year y
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.5	0
Description of measurement methods and procedures to be applied:	The consumption will be measured by a continuous electricity / flow meter, with data aggregated monthly.
QA/QC procedures to be applied:	The flow meter will be calibrated according to appropriate industry/international standards.
Any comment:	Used for the calculation of $PE_{energy_cons,y}$

Data / Parameter:	CO_2EF_{elec}
Data unit:	tCO ₂ /MWh
Description:	CO ₂ emission factor for electricity consumed at project site
Source of data to be used:	EGAT/EPPO/DEDE
Value of data applied for the purpose of calculating expected emission reductions in section B.5	N/A
Description of measurement methods and procedures to be applied:	Calculated as per AMS-I.D
QA/QC procedures to be applied:	N/A – data are obtained from official sources
Any comment:	Used for the calculation of $PE_{energy_cons,y}$

Data / Parameter:	$Q_{biogas_burner,y} / Q_{biogas_flare,y}$
Data unit:	m ³ biogas/h
Description:	Volumetric flow rate of the biogas in dry basis at normal conditions in the hour h
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.6	N/A – for the purpose of <i>ex ante</i> estimation, $Q_{biogas_burner,y}$ and $Q_{biogas_flare,y}$ were used.
Description of	This parameter will be continuously measured by a flow meter. The same basis



measurement methods and procedures to be applied:	(dry or wet) is considered for this measurement and the measurement of volumetric fraction of all components in the biogas ($f_{v,i,biogas,h}$) when the biogas temperature exceeds 60°C. Value to be averaged hourly or at a shorter time interval.
QA/QC procedures to be applied:	Flow meters are to be periodically calibrated according to the manufacturer's recommendation.
Any comment:	Used for the calculation of $PE_{stack,y}$

Data / Parameter:	T_{flare}
Data unit:	°C
Description:	Temperature of the exhaust gas of the flare
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.6	N/A
Description of measurement methods and procedures to be applied:	This parameter will be measured in the flare by a Type N thermocouple. A temperature above 500°C indicates that a significant amount of gases are still being burnt and that the flare is operating. If there is no record of the temperature of the exhaust gas of the flare or if the recorded temperature is less than 500 °C for any particular hour, it shall be assumed that during that hour the flare efficiency is zero.
QA/QC procedures to be applied:	Thermocouples should be replaced or calibrated every year.
Any comment:	Used for the calculation of $PE_{stack,y}$

Data / Parameter:	Flare operation parameter
Data unit:	min/h
Description:	Minutes that flare is detected during the hour h
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.6	0
Description of measurement methods and procedures to be applied:	Measured continuously using a flame detector
QA/QC procedures to be applied:	
Any comment:	Used for the calculation of $PE_{stack,y}$



Data / Parameter:	T
Data unit:	°C
Description:	Temperature of the biogas
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.6	N/A – not estimated <i>ex ante</i> as density assumed to be $0.00065\text{tCH}_4/\text{m}^3\text{CH}_4$. However, temperature after blowers is 60 – 70°C.
Description of measurement methods and procedures to be applied:	This parameter will be measured continuously/periodically by a meter. The measured data is used to determine the density of methane ρ_{CH_4} . No separate monitoring of temperature is necessary when using flow meters that automatically measure temperature and pressure, expressing biogas volumes in normalized cubic meters.
QA/QC procedures to be applied:	Meter will be subject to a regular maintenance and calibrated in accordance with the national or international approved standards and procedures.
Any comment:	Used for the calculation of $PE_{\text{stack},y}$

Data / Parameter:	P
Data unit:	bar
Description:	Pressure of the biogas
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.6	N/A – not estimated <i>ex ante</i> as density assumed to be $0.00065\text{tCH}_4/\text{m}^3\text{CH}_4$. However, pressure after blowers is approximately 450mb g.
Description of measurement methods and procedures to be applied:	This parameter will be measured continuously/periodically by a meter. The measured data is used to determine the density of methane ρ_{CH_4} . No separate monitoring of temperature is necessary when using flow meters that automatically measure temperature and pressure, expressing biogas volumes in normalized cubic meters.
QA/QC procedures to be applied:	Meter will be subject to a regular maintenance and calibrated in accordance with the national or international approved standards and procedures.
Any comment:	Used for the calculation of $PE_{\text{stack},y}$

Data / Parameter:	$Q_{\text{burner_stack},y}$
Data unit:	m^3/yr
Description:	Amount of burner stack gas in year y
Source of data to be used:	SQS, directly measured
Value of data applied for the purpose of	N/A – for the purpose of the <i>ex ante</i> estimation, $PE_{\text{stack},y}$ was approximated as a percentage of methane fed to the burner.



calculating expected emission reductions in section B.6	
Description of measurement methods and procedures to be applied:	This parameter will be obtained from the flow rate of the burner stack gas and the amount of time the gas is combusted in the burner.
QA/QC procedures to be applied:	Standard calibration will be carried out.
Any comment:	Used for the calculation of $PE_{stack,y}$

Data / Parameter:	$W_{CH_4_stack}$
Data unit:	m^3CH_4/m^3 stack gas
Description:	Fraction of methane in burner stack gas
Source of data to be used:	SQS or outside laboratory, directly measured
Value of data applied for the purpose of calculating expected emission reductions in section B.6	0.995
Description of measurement methods and procedures to be applied:	This parameter will be measured at least quarterly, in line with AM0013.
QA/QC procedures to be applied:	Meter will be subject to a regular maintenance and calibrated in accordance with the national or international approved standards and procedures. If outsourced, the outside entity should be ISO17025 accredited.
Any comment:	Used for the calculation of $PE_{stack,y}$

Data / Parameter:	Regulations and incentives relevant to wastewater
Data unit:	-
Description:	Thai regulations and/or incentives relevant to wastewater that may impact the baseline
Source of data to be used:	Thai official documents
Value of data applied for the purpose of calculating expected emission reductions in section B.5	N/A
Description of measurement methods and procedures to be applied:	Will be assessed at the renewal of the crediting period
QA/QC procedures to	N/A



be applied:	
Any comment:	N/A

B.7.2 Description of the monitoring plan:

SQS will appoint an executive to be responsible for all data monitoring, acquisition and recording for CDM purposes. Staff have been trained in the operation of all monitoring equipment and all readings will be taken in a systematic and transparent manner under the supervision of management. Quality control and assurance procedures are to be undertaken for data monitored as outlined in the monitoring plan. A database will be maintained to record all relevant data as in the monitoring plan. Such monitoring procedures and management structure will be in accordance with the ISO 9001, which SQS is accredited for.

The management team will review the data archived and submit a complete set of documentation, which indicates the calculation procedure as well as the *ex post* emission reduction estimate, to the general manager regularly. In addition to the internal verification by general manager, this properly recorded documentation will also be verified externally by an independent Designated Operational Entity (DOE) on an annual basis.



Figure 4: Entrance to SQS factory showing ISO certification

B.8 Date of completion of the application of the baseline study and monitoring methodology and the name of the responsible person(s)/entity(ies)

The baseline study was completed in April 2007 by MUS.

Clean Energy Finance Committee
Mitsubishi UFJ Securities Co., Ltd.
Tokyo, Japan
Phone: +81-3-6213-6331
E-mail: hatano-junji@sc.mufg.jp; ktochikawa@cefconsulting.com



MUS is a project participant as defined by the CDM Executive Board. Contact details are provided in Annex 1.



SECTION C. Duration of the project activity / crediting period

C.1 Duration of the project activity:

C.1.1. Starting date of the project activity:

31/03/2005

C.1.2. Expected operational lifetime of the project activity:

12 years

C.2 Choice of the crediting period and related information:

C.2.1. Renewable crediting period

C.2.1.1. Starting date of the first crediting period:

This section is intentionally left blank.

C.2.1.2. Length of the first crediting period:

This section is intentionally left blank.

C.2.2. Fixed crediting period:

C.2.2.1. Starting date:

10/10/2008 or from the date of registration, whichever is later.

C.2.2.2. Length:

10 years

**SECTION D. Environmental impacts****D.1. Documentation on the analysis of the environmental impacts, including transboundary impacts:**

The Project will contribute to the following major positive environmental impacts:

- Improvement of local air quality – odour. One of the major problems associated with wastewater treatment is the pungent odour arising from the open lagoons, during the long decomposition process. By treating the wastewater from the starch factory in a digester that allows accelerated decomposition in a controlled environment, this will significantly improve the air quality, which is important not only beyond the SQS factory's borders, but also to SQS staff within the grounds.
- Improvement of local air quality – fossil fuel. By using the methane contained in the recovered biogas, the Project taps into an unused, environmentally friendly and renewable energy source. In doing so, it will reduce the consumption of fuel oil at the SQS factory.
- Improvement of security of local ground water. Since the biodigester is lined and covered with PE sheet, there is greater security against leakage of waste water into the water sources around the factory compared with open lagoons which could seep or overflow. This has proven to be an important point with the local stakeholders.

No negative impacts are identified with the Project.

It is noted that as SQS will adhere to its environmental management plan for continuous improvement, in accordance with its ISO14001 accreditation.

D.2. If environmental impacts are considered significant by the project participants or the host Party, please provide conclusions and all references to support documentation of an environmental impact assessment undertaken in accordance with the procedures as required by the host Party:

Under Thai regulations, no environmental impact assessment or equivalent were required for the project activity.

**SECTION E. Stakeholders' comments****E.1. Brief description how comments by local stakeholders have been invited and compiled:**

SQS invited local leaders to inspect its factory premises on May 2, 2006. A total of 38 persons, including the management and committee members of the Khokrengrom and Khokphechrphattana Tambol Administrative Councils⁹ and a Kamnan and Village Head from the Khokrengrom area attended the session. SQS was represented by the following personnel:

Mr. Weerasit Mahattanakhun	Assistant Administration.Division Manager
Mr. Sampart Rerkchawee	Engineering Section Manager
Mr. Wiratn Wosri	Assist. Personnel Section Manager
Ms. Phentip Jatunawaratn	Quality Control Officer
Ms. Saengduan Em-O	Quality Systems Officer
Mr. Pleumjit Buasri	Project Engineer
Mr. Anant Thipprathum	Electrical Technician
Mr. Nikul Jekthao	Mechanical Technician
Mr. Sura Narongchai	Personnel Officer

The session included:

- Opening remarks by Mr. Weerasit Mahattanakhun
- A video presentation about SQS
- A presentation of Production Facilities
- A presentation of Wastewater Treatment System
- A presentation of Biogas Plant
- Inspection of the Factory

⁹ A Tambol consists of a cluster of 5 - 10 villages



Figure 5: The presentation of the Project by the Engineering Section Manager



Figure 6: Visitors inspecting the biogas plant

E.2. Summary of the comments received:

Two main issues were raised during the session:



1. It was requested that SQS stop discharge of all water, including rainwater, to the nearby irrigation canal to ensure no contamination of the water;
2. The bad smell from the wastewater treatment plant is causing nausea to people in the new village of Somboon Wattana during the rainy season and when prevailing winds blow in that direction;

Other issues such as payment to local farmers for the tapioca root and local taxes were also discussed.

E.3. Report on how due account was taken of any comments received:

1. In response to the complaint of discharge, the participants were invited to inspect the wastewater channel and shown how soil subsidence caused runoff into the nearby creek. It was explained that this fault had been rectified and the participants were also informed of measures that would prevent a repetition of the runoff. Moreover, the participants made their own recommendations on how to prevent rainwater from flowing into the irrigation channel, which is mistaken for wastewater discharge, and SQS made a commitment to following their recommendations in the future;
2. It was explained to the attendees that by installing an advanced system which will allow for a faster treatment of wastewater in an enclosed environment, the Project will dramatically reduce the bad odour affecting the villagers. This was received enthusiastically by the participants;

As a result of the session, the local representatives were impressed that SQS was willing to take the lead in implementing an advanced solution to not only effectively treat wastewater but one that would drastically reduce the bad odour. They were satisfied that they will be able to report back positively to villagers to whom they are ultimately accountable.

**Annex 1****CONTACT INFORMATION ON PARTICIPANTS IN THE PROJECT ACTIVITY**

Organization:	Siam Quality Starch Company Limited (Project Owner)
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URL:	http://www.sc.mufg.jp/english/e_cefc/
Represented by:	
Title:	Secretary, Clean Energy Finance Committee
Salutation:	Mr.
Last Name:	Toyofuku
Middle Name:	
First Name:	Masayuki
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Annex 2

INFORMATION REGARDING PUBLIC FUNDING

The Project does not involve funding from an Annex I country.



Annex 3

BASELINE INFORMATION

Please refer to Section B.6. for details.



Annex 4

MONITORING INFORMATION

Please refer to Section B.7. for details.

1. Data archiving

All data will be archived on paper and/or electronically, and kept until 2 years after the end of the crediting period.

2. Emergency procedures

Emergency procedures in terms of both monitoring and operation are in place, in accordance with ISO9001.
