



CDM – Executive Board

Revised Monitoring Plan

(UNFCCC Reference Number 0677)

Project Title

Optimization of steam consumption by applying retrofit measures in blow heat recovery system

Version 1 07-07-2008



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PROJECT DESIGN DOCUMENT FORM (CDM PDD) - Version 02



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SECTION D. Application of a monitoring methodology and plan

D.1. Name and reference of <u>approved monitoring methodology</u> applied to the <u>project activity</u>:

Title: Steam Optimization System, AM0018: version 1, Sectoral Scope: 3, 6 December 2004; Reference: website of CDM UNFCCC - Approved baselines and monitoring methodologies for CDM project

D.2. Justification of the choice of the methodology and why it is applicable to the project activity:

As discussed earlier in the Section B.2, the applicability conditions of the methodology are applicable to the proposed CDM project. Thus, in conjunction with the baseline methodology, the monitoring methodology has also been applied to the project.

The monitoring methodology is applicable to the project activity as the parameters to be monitored is relevant to the project activity and project activity proposes to follow the monitoring methodology as provided in the tables below.



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D	D.2. 1. Option 1: Monitoring of the emissions in the project scenario and the <u>baseline scenario</u>											
	D.4.1	1		• • • •				A. T. M. T. T. T.				
	D.2.1.	I. Data to be	collected	in order to monit	tor emissions fr	om the <u>proje</u>	ect activity, and h	ow this data will be archived:				
ID number	Data variable	Source of data	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportio n of data to be monitore d	How will the data be archived? (electronic/ paper)	Comment				
E _{quip P}	Rated Power of the spray condenser pump	Supplier document having Name plate details	kW	E	Once during installation	100%	Electronic/ paper	The unit has recorded the rated power of the spray condenser pump (supplier document) which has been additionally installed due to project activity.				
BHRS _{hrs}	Running hours of the BHRS	Constant	hrs	С	Calculated for the given period	100%	Electronic	As the hours of operation of the BHRS is required to calculate the operating hours of the additional condenser pump additionally installed due to project activity leading to project emissions, it is conservatively assumed that the pump would have run for 24X7 for the given period. This would lead to higher consideration of project emission and thus conservative calculation of net emission reduction from the project activity.				
E _{add}	Additional electricity consumed by the project activity	Monitoring report	GWh	С	For the monitoring period	100%	Electronic/Pap er	The additional electricity consumed by the project activity would be calculated in million units (GWh) as rated power of the additional condenser pump (30kW) multiplied with number of days of operation for the given monitoring period into 24 hours in a day divided by 10^6.				
EF _{elec}	Emission factor of the electricity used in the project activity	Using in plant records	tCO2/ GWh	С	Once during PDD completion	100%	Electronic/Pap er	The grid emission factor is calculated based on methodology ACM0002 version 06. For in-house electricity emission factor calculation, proposed equation has been applied (given below). It is proposed that the emission factor of the electricity used by the project activity would be estimated only once during PDD completion. This is considered to be conservative because: - 1. Grid contribution to the total electricity consumed by				



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the unit is only 5% and most likely to reduce further as the unit strives to be self sufficient. 2. The in-house generation is based on coal and biomass and the unit plans to increase the biomass contribution to the total capacity. Thus the emission factor of the in-house electricity is likely to drop. Therefore, it is conservative to keep the emission factor constant this is used for calculation of project emissions.									
									 the unit is only 5% and most likely to reduce further as the unit strives to be self sufficient. The in-house generation is based on coal and biomass and the unit plans to increase the biomass contribution to the total capacity. Thus the emission factor of the in-house electricity is likely to drop. Therefore, it is conservative to keep the emission factor constant this is used for calculation of project emissions.
									eenstant and is about for our our our project enhostens.
D 2 1.2 Description of formulae used to estimate project emissions (for each gas, source, formulae/algorithm, emissions units of CO, equ.)	Г	111 Deseri	ntion of form	ilao usod i	o ostimato proio	at amissions (f	or oach gas	ourse formulael	algorithm amissions units of CO agu
D.2.1.2. Description of formulae used to estimate project emissions (for each gas, source, for mulae/algorithm, emissions units of CO ₂ equ.)	L	J.2.1.2. Desch	puon or form	liae useu	to estimate proje	ect emissions (1	or each gas, s	ource, for mulae/a	algorithm, emissions units of CO ₂ equ.)
»>	>>								
$\operatorname{Cer}_{p} = \operatorname{E}_{\operatorname{add}} x \operatorname{EF}_{\operatorname{elec}} $ (1)	Cer _p =	= E _{add} x EF _{elec}							(1)
Where	Where								
$Cer_{n} = CO_{2}$ emissions due to project activity (tCO ₂)	$Cer_n = CC$	D ₂ emissions du	e to project act	ivity (tCO	,)				
$E_{\rm ev} = {\rm Additional electricity consumed by the project (GWh) and calculated as: -$	$F_{ab} = Adc$	ditional electric	ity consumed h	w the proi	ect (GWh) and ca	lculated as: -			

(2)

 $E_{add} = E_{quipP} * BHRS_{hrs} / 10^{6}$

Where:

 E_{quipP} = Rated power of the spray pump (30 kW) BHRS_{hrs} = Operating hours of the blow heat recovery system (hrs) calculated as number of days of operation for the given monitoring period into 24 hours in a day

EF _{elec} = (EF _{in-house} * EG _{in-house}) + (EF _{grid} * EG _{grid}) / (EG _{grid} + EG _{in-house})	(3)
Where	
$EF_{elec} = Emission$ factor for the electricity used by the project activity (tCO ₂ /GWh) (constant – 1275tCO2/GWh)	
$EF_{in-house} = Emission factor of the electricity generated in-house (tCO2/GWh)$	
EF _{orid} = Emission factor of the gird electricity imported by the unit (tCO ₂ /GWh)	
EG _{orid} = Total grid electricity used by the unit (GWh)	
$EG_{in-house}^{fin}$ = Total in-house electricity generated by the unit (GWh)	
$EF_{erid} = \sum FF_{i,v} * COEF_i / \sum Gen_{f,i,v}$	(4)
Where:	
FF_{iy} = Last 3 years average of fuel energy consumed by plant 'P' of type 'i'(TJ)	
$COEF_i = Carbon-dioxide emission factor of fuel type 'i'(tCO_2/TJ)$	
\sum Gen _{Piv} = Total generation by plant 'P' using fuel 'i' in the last 3 years (average) (GWh)	
$\mathbf{EF}_{\text{in-house}} = ((\mathbf{S}_{\text{tot}} * \mathbf{E}_{s})/\eta_{b}) * \mathbf{COEF}_{\text{coal}} * \mathbf{O}_{\text{CFB}} / \mathbf{E}_{\text{in-house}}$	(5)
Where:	
S_{tot} = Total steam consumed for in-house electricity generation	

 E_s = Net enthalpy of the steam (kcal/kg) used for generation of electricity and calculated as per equation 15



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 $\begin{array}{l} \eta_b = A \mbox{verage efficiency (\%) of the steam producing boilers calculated as per approved methodology using direct method \mbox{\%H}_{CFB} = Operating hours of the coal fired boiler (\%) \\ COEF_{coal} = Carbon-dioxide emission factor of coal (tCO_2/TJ) \\ E_{in-house} = Total electricity generated in-house \end{array}$

	D.2.1.3. Relevant data necessary for determining the <u>baseline</u> of anthropogenic emissions by sources of GHGs within the project boundary and											
how such	h data will b	e collected	and arc	hived :								
ID	Data	Source	Data	Measured	Recording	Proportion	How will the data	Comment				
number	variabl	of data	unit	(m),	frequency	of data to	be archived?					
	e			calculated (c),		be	(electronic/ paper)					
				estimated (e),		monitored						
At Basel	ine Scenario											
P _{rep}	Hot water	In-plant	MT	М	Measured per shift for a month	100%	Electronic/paper	The generation of hot-water is monitored through the connected distribution control system (DCS) and				
	at the				prior to the			recorded per shift basis in the in-plant shift log book by				
	baseline				implementation			the operator / shift in-charge Daily aggregates are then				
					of the project			logged into online Integrated Management Information				
					F J			System (IMIS). Archived – For crediting period plus 2				
								years				
Sren	Correspon	In-plant	MT	М	Measured per	100%	Electronic/paper	-do as above -				
	ding				shift for a month							
	steam				prior to the							
	consumpti				implementation							
	on				of the project							
SSCR	Specific	Project	MT/	С	Once during	100%	Electronic/Paper	Archived – For crediting period plus 2 years				
	steam	Excel-	MT		PDD completion							
	consumpti	sheet										
	on											
At the pr	oject scenari	0										
P _{rep1}	Hot	In-plant	MT	М	Per shift	100%	Electronic/ paper	The generation of hot-water is monitored through the				
	water							connected distribution control system (DCS) and				
	generati							recorded per shift basis in the in-plant -shift log book				
	on at		1					by the operator / shift in-charge. Daily aggregates are				
	the		1					then logged into online Integrated Management				
	project							Information System (IMIS). Archived – For crediting				
	scenario							period plus 2 years				



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	D.2.1.3. Relevant data necessary for determining the <u>baseline</u> of anthropogenic emissions by sources of GHGs within the project boundary and												
how such	data will b	e collected	and arch	nived :	1	-	1						
ID number	Data variabl e	Source of data	Data unit	Measured (m), calculated (c), estimated (e),	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	Comment					
S _{rep1}	Corresp onding steam consum ption	In-plant	MT	M	Per shift	100%	Electronic/ paper	-do as above-					
SSCR ₁	Corresp onding specific steam consum ption	Emissio n calculati on sheet	MT/ MT	С	As and when emission is calculated	100%	Electronic / paper	Archived – For crediting period plus 2 years					
Es	Net enthalp y of the steam	Emissio n calculati on sheet	kcal/k g	С	As and when emission is calculated	100%	Electronic/paper	Enthalpy of the steam at the boiler outlets is determined based on steam table which is a matrix of steam properties with corresponding values of steam pressure and temperature. The net enthalpy of the steam is determined by subtracting feed water enthalpy from the gross steam enthalpy. This parameter is calculated based on daily data of steam pressure and temperature, and feed water flow and temperature					
Steam pressure	Steam pressure at the boiler end	In-plant records	kg/cm (gaug e)	М	Per-shift	100%	Electronic/ paper	The steam pressure at the boiler end is measured with dedicated pressure gauges. The pressure gauges are monitored through dedicated DCS and values are recorded on per shift basis and archived in IMIS on daily basis.					
Steam temperat ure	Steam tempera ture at the boiler end	In-plant records	°C	M	Per-shift	100%	Electronic/ paper	The steam temperature at the boiler end is measured with dedicated thermocouple. The thermocouples are monitored through dedicated DCS and values are recorded on per shift basis and archived in IMIS on daily basis.					

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	D.2.1.3. Relevant data necessary for determining the <u>baseline</u> of anthropogenic emissions by sources of GHGs within the project boundary and												
how such a	data will b	e collected	and arcl	nived :									
ID	Data	Source	Data	Measured	Recording	Proportion	How will the data	Comment					
number	variabl	of data	unit	(m),	frequency	of data to	be archived?						
	e			calculated (c),		be	(electronic/ paper)						
				estimated (e),		monitored							
Feed water flow	Feed water flow to the steam boilers	In plant records	MT	М	Monthly	100%	Electronic/ paper	The feed water inlet to the boiler is measured with dedicated flow meter. The meters are monitored through dedicated DCS and archived in IMIS on daily basis.					
Feed water temperat ure	Feed water tempera ture	Emissio n calculati on sheet	°C	М	Monthly	100%	Electronic/ paper	The feed water temperature at the boiler end is measured with dedicated thermocouple. The thermocouples are monitored through dedicated DCS					
H _{boiler,i}	Operati ng hours of the boiler by fuel type 'i'	Mill perform ance report	Hours	C	Monthly	100%	Electronic/ paper	The actual operating hours of the boilers are calculated on daily basis by subtracting the recorded downtime (in log-sheets/ IMIS report) from the total operating hours possible in a given month considering 24hours of operation per day.					
S _{tot}	Total steam produce d by the boilers	Mill perform ance report	MT	М	Monthly	100%	Electronic/ paper	The steam generated by the boilers is measured with dedicated steam flow meters. The meters are monitored through dedicated DCS and archived in IMIS.					

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_	D.2	1.3. Relev	ant data	necessary for de	termining the <u>b</u> a	aseline of anthr	opogenic emissions by	sources of GHGs within the project boundary and		
how such	data will b	e collected	and arc	hived :	Т			1		
ID number	Data variabl e	Source of data	Data unit	Measured (m), calculated (c), estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	Comment		
F _{tot,i}	Total amount of fuel used for steam generati on by type 'i'	Mill perform ance report	MT	M	Monthly	100%	Electronic/ paper	Two types of fuel are used, namely, coal and black liquor solids. Coal – measured using weigh bridge and stock method BLS - Measured on daily basis and computed on monthly basis in IMIS. The installed meter reads the flow of black liquor in mass. To ascertain the % of solids in the biomass fuel, samples are tested in the in-house laboratory and accurate amount of biomass flow is determined based on volumetric flow multiplied by the % solids determined by the lab results. The density factor used to convert to mass is 1.35.	-	
NCV _i	Net calorific value of the fuel by type 'i'	Emissio n calculati on sheet	Kcal/ kg	₩	_Monthly	100%	_ Electronic/ paper	Internal fuel test Procedure: Ash and moisture content in the coal sample is tested as per procedure and values are substituted in the formula to arrive at GCV. The net calorific value of the coal used will be calculated based on GCV and moisture percentage. (NCV = GCV – 10.02*M), Ultimate analysis for coal is also done with third party on monthly basis. NCV for BLS will be determined by third party on dry basis.		Deleted: C Deleted: determined through ultimate analysis of the fue Deleted: subtracting the
ηboiler	Average	Emissio	%	e	Monthly	100%	Electronic/ paper	Average efficiency of the steam generating boilers is	, ,	Deleted: content
	efficien	n		<u></u>				calculated using formula inline with the approved	1	Deleted:
	cy of	calculati						methodology by applying Direct Boiler Efficiency		Deleted: C
	the steam generati ng boilers	on sheet						Method (Input-Output Method)		Deleted: This parameter is calculated based on daily data of steam pressure and temperature, and feed water flow and temperature, fuel consumption by type and the net calorific values

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D.2.1.3. Relevant data necessary for determining the <u>baseline</u> of anthropogenic emissions by sources of GHGs within the project boundary and												
how such data will be collected and archived :												
ID	Data	Source	Data	Measured	Recording	Proportion	How will the data	Comment]			
number	variabl	of data	unit	(m),	frequency	of data to	be archived?					
	e			calculated (c),		be	(electronic/ paper)					
				estimated (e),		monitored						
Fc	Carbon	Third	v	<u>m</u>	Monthly	100%	paper	Carbon percentage in the coal is analysed through third				
	content	party	% on					party report	×			
	of the	analysis	weigh						$\left \cdot \right\rangle$			
	coal	report	<u>t</u>			1	L		<u>``</u>			
			basis									

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Deleted: emission factor of the coal used for generation of steam.

D.2.1.4. Description of formulae used to estimate baseline emissions (for each gas, source, formulae/algorithm, emissions units of CO ₂ equ.)									
»»									
$Prep = (P_1 + P_2 + P_m) x A / m$	(6)								
Where									
P_{rep} = Representative production for the day at the baseline for a period of a month prior to implementation of the project (MT) P_1, P_2,P_m = shift-wise hot water production (MT) for a period of a month prior to implementation of the project A = number of shifts/day (constant 3) m = number of shifts in that particular month									
Srep = $(S_1 + S_2 \dots + S_z) \times A/z$ Where	(7)								
$S_{rep1} =$ Representative steam consumption for the day (corresponding to Prep) at baseline for a period of a month p $S_1, S_2,, S_m =$ shift-wise steam consumption values, corresponding to P1,Pm A = number of shift/day (constant 3) z = number of shifts in that particular month	rior to implementation of the project (MT)								
SSCR = Srep/ Prep	(8)								
Where									
SSCR = Specific Steam Consumption Ratio at baseline (MT/MT)									
Prep ₁ = $(P_1 + P_2 \dots + P_m) \times A / m$ Where	(9)								
P_{rep1} = Representative production for the day (MT) and then aggregated for a month P_1, P_2, \dots, P_m = shift-wise hot water production (MT)									
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A = number of shifts/day (constant 3) m = number of shifts in the given period	
$\begin{array}{l} Srep_1 &= (S_1 + S_2 \dots + S_z) \ x \ A/z \\ Where \\ S_{rep1} &= Representative steam consumption for the day (corresponding to Prep_1) (MT) \\ S_1, S_2, \dots S_m &= shift-wise steam consumption (MT) corresponding to P1, \dots Pm \\ A &= number \ of \ shift/day \ (constant \ 3) \\ z &= number \ of \ shifts \ in \ the \ given \ period \end{array}$	(10)
$SSCR_1 = Srep_1 / Prep_1$ Where	(11)
$SSCR_1$ = Average specific steam consumption ratio for the given period (MT/MT)	
SSCR _{diff} = SSCR - SSCR ₁	(12)
SSCR _{diff} = difference in specific steam consumption ratio from baseline and project scenario (MT/MT)	
$S_{net} = SSCR_{diff} x P_{act}$ Where	(13)
S_{net} = Actual reduction in steam consumption for the given period (MT) P_{act} = Actual hot water generation for the given period (MT)	
$\mathbf{E}_{\text{net}} = \mathbf{S}_{\text{net}} \mathbf{x} \mathbf{E}_{\text{s}}$	(14)
$E_{net} = Net reduction in steam energy consumption (kCal)$	
S_{net} = Net reduction in steam consumption (MT) E_s = Net enthalpy of steam being supplied (kCal/kg).	
and $\mathbf{E}_{s} = \mathbf{E}_{tot} - \mathbf{E}_{fw}$	(15)
where $F_{m} = Gross enthalpy of steam at the boiler outlet (kCal/kg)$	
E_{fw} = Heat content of feed water (kCal/kg)	
$\mathbf{E}_{in} = \mathbf{E}_{net} / \eta \mathbf{b}$ Where	(16)
E_{in} = Total fuel energy saved by the project for the given period (TJ) ηb = Efficiency of boiler, to be monitored periodically by direct method (%) as per methodology	

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 $\begin{bmatrix} C_{er} = E_{in} x \sum (EF_{fuel} x \% H fuel) \\ Where \end{bmatrix}$

 $C_{er} = CO_2$ emission reductions for the given period (tCO₂e)

 EF_{fuel} = Carbon emission factor for fuel by type 'i' (tCO₂/TJ)

 $%H_{fuel} = %$ of hours of operation of the boiler with fuel by type 'i'.

D. 2.2. Option 2: Direct monitoring of emission reductions from the <u>project activity</u> (values should be consistent with those in section E).

D.2.2.1. Data to be collected in order to monitor emissions from the <u>project activity</u> , and how this data will be archived:												
ID number	Data	Source of	Data	Measured (m),	Recording	Proportion	How will the data	Comment				
	variable	data	unit	calculated (c),	frequency	of data to	be archived?					
				estimated (e),		be	(electronic/					
						monitored	paper)					

NOT APPLICABLE

D.2.2.2. Description of formulae used to calculate project emissions (for each gas, source, formulae/algorithm, emissions units of CO2 equ.):

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NOT APPLICABLE

D.2.3. Treatment of <u>leakage</u> in the monitoring plan D.2.3.1. If applicable, please describe the data and information that will be collected in order to monitor <u>leakage</u> effects of the <u>project activity</u>											
ID number	Data variable	Source of data	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	Comment			

D.2.3.2. Description of formulae used to estimate leakage (for each gas, source, formulae/algorithm, emissions units of CO2 equ.)

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Not applicable project emission has already been accounted.



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D.2.4. Description of formulae used to estimate emission reductions for the project activity (for each gas, source, formulae/algorithm, emissions units of CO₂ equ.)

(18)

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 $C_{ernet} = C_{er} - C_{er,p}$ Where

 C_{ernet} = Net CO₂ emission reductions due to the project (tCO₂e) C_{er} = CO₂ emission reductions due to the project (tCO₂e) C_{erP} = CO₂ emissions attributable to the project activity (tCO₂e)

D.3.	Quality control (QC) and quality assurance (QA) procedures are being undertaken for data monitored	
Data	Uncertainty level of data (High/Medium/Low)	Explain QA/QC procedures planned for these data, or why such procedures are not necessary.
All	Medium to low	All data will be monitored under recorded under ISO system, which undergoes periodic review once in three month, internally, and bi-annually by third party. Where relevant the meters and equipments will be calibrated as per schedule (once in a year) internally. For those where internal facilities are not available such as calibration, fuel analysis will be done through external accredited agencies.



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D.4 Please describe the operational and management structure that the project operator will implement in order to monitor emission reductions and any <u>leakage</u> effects, generated by the <u>project activity</u>

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ITC PSPD had deputed a team of qualified engineers to conceive, install and make operational the whole project. The General Manager (technical) would be assisted by his group of service and maintenance managers to implement the monitoring plan. The management structure for this project would be integrated with the ISO system in vogue at the plant.

D.5 Name of person/entity determining the monitoring methodology:

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Date of completion of monitoring plan - 07-07-08

Entity determining monitoring methodology: CDM Project Developer – M/s PricewaterhouseCoopers Pvt. Ltd. Not project participants.