

**Draft revision** to the approved baseline and monitoring methodology AM0021**“Baseline Methodology for decomposition of N<sub>2</sub>O from existing adipic acid production plants”****I. SOURCES AND APPLICABILITY****Source**

This methodology is based on the N<sub>2</sub>O Emission Reduction Project in Onsan, Republic of Korea, whose baseline study, monitoring and verification plan and project design document were prepared by Rhodia Energy SAS, France, Rhodia Polyamide Intermediate SAS France, and Perspective Climate Change, Germany. For more information regarding the proposal and its consideration by the Executive Board please refer to case NM0061: “N<sub>2</sub>O Emission Reduction Project in Onsan” on <http://cdm.unfccc.int/methodologies/PAMethodologies/approved.html>.

This methodology also refers to the latest approved versions of the following tools:

- “Tool to calculate baseline, project and/or leakage emissions from electricity consumption”;
- “Tool to calculate project or leakage CO<sub>2</sub> emissions from fossil fuel combustion”;
- “Tool for the demonstration and assessment of additionality”.

**Selected approach from paragraph 48 of the CDM modalities and procedures**

“Existing actual or historical emissions as applicable”

**Applicability**

This methodology is applicable to project activities that consist of the installation of a new dedicated N<sub>2</sub>O decomposition facility at existing adipic acid production plants.<sup>1</sup> The N<sub>2</sub>O destruction facility could be either catalytic or thermal decomposition, and will convert the nitrous oxide into nitrogen, and thereby prevent its release to the atmosphere.

The methodology is applicable only for existing production capacity of adipic acid where the commercial production had begun by 31 December 2004.

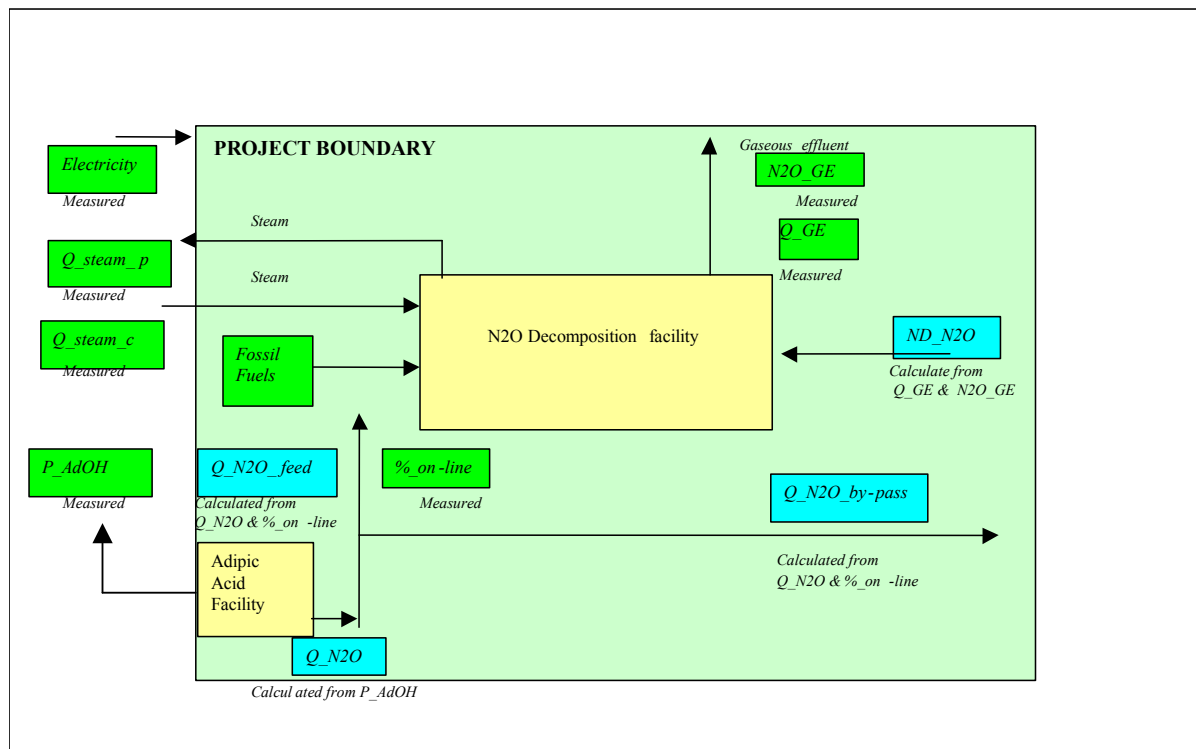
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<sup>1</sup> Production of adipic acid generates N<sub>2</sub>O as a by-product. Nitrous oxide (N<sub>2</sub>O) is typically released into the atmosphere as it does not have any economic value.

## II. BASELINE METHODOLOGY PROCEDURE

### Project Boundary

The spatial extent of the project boundary is the site of the adipic acid production facility and N<sub>2</sub>O decomposition facility. Schematic illustration of the project boundary is provided in Figure 1 below.



**Figure 1: Schematic illustration of the project boundary**

Gases and sources considered in the project boundary are provided in Table 1 below.

**Table 1: Summary of gases and sources included in the project boundary, and justification/explanation where gases and sources are not included:**

	Source	Gas	Included?	Justification / Explanation
Baseline	Emissions from adipic acid production process	CO <sub>2</sub>	Yes	Emissions from steam that would have been produced in absence of the project activity
		CH <sub>4</sub>	No	Not applicable
		N <sub>2</sub> O	Yes	The main source of emissions
Project Activity	Emissions from adipic acid production process	CO <sub>2</sub>	No	Not applicable. In project activity steam is generated as a by-product of decomposition process.
		CH <sub>4</sub>	No	Not applicable
		N <sub>2</sub> O	Yes	N <sub>2</sub> O emissions from process that are directly released in the atmosphere during project activity and residual N <sub>2</sub> O in the exhaust of decomposition facility
	Emissions related to the production of ammonia used for NO <sub>x</sub> reduction <sup>2</sup>	CO <sub>2</sub>	Yes	To be considered where no SCR De NO <sub>x</sub> - is installed and operational prior to the project start
		CH <sub>4</sub>	No	Not applicable
		N <sub>2</sub> O	No	Not applicable
	Emissions from use of fossil fuels in the N <sub>2</sub> O destruction facility	CO <sub>2</sub>	Yes	CO <sub>2</sub> emissions from the onsite use of fossil fuels can be significant
		CH <sub>4</sub>	No	CH <sub>4</sub> emissions are assumed to be very small. Excluded for simplification.
		N <sub>2</sub> O	No	N <sub>2</sub> O emissions are assumed to be very small. Excluded for simplification.
	Emissions from use of electricity in the N <sub>2</sub> O destruction facility	CO <sub>2</sub>	Yes	CO <sub>2</sub> emissions from on site use of electricity can be significant.
		CH <sub>4</sub>	No	CH <sub>4</sub> emissions are assumed to be very small. Excluded for simplification.
		N <sub>2</sub> O	No	N <sub>2</sub> O emissions are assumed to be very small. Excluded for simplification.

**Identification of baseline scenario**

Baseline scenario shall be identified following the procedure given below:

**Step 1: Identify all realistic and credible alternatives to the project activity:**

The baseline scenario alternatives should include all technically feasible options which are realistic and credible.

<sup>2</sup> Attention: Ammonia used for NO<sub>x</sub> reduction does not cause GHG emissions, only the production of ammonia causes GHG emissions.



***Sub-step 1a: The baseline scenario alternatives should include all possible options that are technically feasible to handle N<sub>2</sub>O emissions. These options shall include, inter alia:***

- The continuation of the current situation, where there will be no installation of unit for the destruction or abatement of N<sub>2</sub>O;
- Switch to alternative production methods that avoid production of N<sub>2</sub>O;
- Alternative use of N<sub>2</sub>O such as:
  - Recycling and reuse of N<sub>2</sub>O within the chemical complex;
  - The use of N<sub>2</sub>O for external purposes.
- Installation of a Non-Selective Catalytic Reduction (NSCR) DeNO<sub>x</sub> unit;
- Installation of a N<sub>2</sub>O destruction or abatement technology, i.e., project activity implemented without CDM.

***Sub-step 1b: In addition to the baseline scenario alternatives of Step 1a, all possible options that are technically feasible to handle NO<sub>x</sub> emissions shall be considered, for instance, the installation of a NSCR DeNO<sub>x</sub> unit could also cause N<sub>2</sub>O emission reduction. Therefore NO<sub>x</sub> emission regulations have to be taken into account in determining the baseline scenario. The respective options are, inter alia:***

- The continuation of the current situation, where either a DeNO<sub>x</sub>-unit is installed or not;
- Installation of a new Selective Catalytic Reduction (SCR) DeNO<sub>x</sub> unit;
- Installation of a new NSCR DeNO<sub>x</sub> unit for the purpose of NO<sub>x</sub> reduction;
- Installation of any other new tertiary measure that combines NO<sub>x</sub> and N<sub>2</sub>O emission reduction.

***Step 2: Eliminate baseline alternatives that do not comply with mandatory legal or regulatory requirements:***

- (1) The baseline alternatives shall be in compliance with all applicable legal and regulatory requirements, even if these laws and regulations have objectives other than GHG reductions (N<sub>2</sub>O), e.g. national or local NO<sub>x</sub> regulations or byproduct waste. This step does not consider national and local policies that do not have legally binding status. Eliminate all baseline alternatives that do not comply with the legal and regulatory requirements on N<sub>2</sub>O and NO<sub>x</sub> emissions;
- (2) If an alternative does not comply with all applicable legislation and regulations, then show that, based on an examination of current practice in the country or region in which the law or regulation applies, those applicable legal or regulatory requirements are systematically not enforced and that non-compliance with those requirements is widespread in the country. If this cannot be shown, then eliminate the alternative from further consideration;
- (3) If the proposed project activity is the only alternative amongst the ones considered by the project participants that is in compliance with all regulations with which there is general compliance, then the proposed project activity is the baseline scenario.

**Table 2: Potential baseline scenarios taking legal or regulatory requirements into account:**

<i>Adipic acid Production Plant in compliance with N<sub>2</sub>O and NO<sub>x</sub> regulation</i>	<i>Adipic acid Production Plant not in compliance with NO<sub>x</sub> regulation</i>	<i>Adipic acid Production Plant not in compliance with N<sub>2</sub>O regulation</i>
Continuation Status quo	SCR DeNO <sub>x</sub> installation	SCR De NO <sub>x</sub> installation that combines N <sub>2</sub> O and NO <sub>x</sub> emission reduction
Installation of N <sub>2</sub> O destruction or abatement technology	Installation of NSCR De NO <sub>x</sub> technology	Installation of N <sub>2</sub> O destruction or abatement technology
Alternative use of N <sub>2</sub> O	Destruction method that combines NO <sub>x</sub> and N <sub>2</sub> O emission reduction	Alternative use of N <sub>2</sub> O

***Step 3: Eliminate baseline alternatives that face prohibitive barriers (barrier analysis):***

***Sub-Step 3a: On the basis of the alternatives that are technically feasible and in compliance with all legal and regulatory requirements, the project participant should establish a list of barriers that would prevent alternatives to occur in the absence of CDM. Barriers should include, among others:***

- Investment barriers, *inter alia*:
  - Debt funding is not available for this type of innovative project activity;
  - No access to international capital markets due to real or perceived risks associated with domestic or foreign direct investment in the country where the project activity is to be implemented.
- Technological barriers, *inter alia*:
  - Technical and operational risks of alternatives;
  - Technical efficiency of alternatives (e.g. N<sub>2</sub>O destruction, abatement rate);
  - Skilled and/or properly trained labor to operate and maintain the technology is not available and no education/training institution in the host country provides the needed skill, leading to equipment disrepair and malfunctioning;
  - Lack of infrastructure for implementation of the technology.
- Barriers due to prevailing practice, *inter alia*:
  - The project activity is the “first of its kind”: No project activity of this type is currently operational in the host country or region.

Provide transparent and documented evidence, and offer conservative interpretations of this documented evidence, as to how it demonstrates the existence and significance of the identified barriers. Anecdotal evidence can be included, but alone is not sufficient proof of barriers. The type of evidence to be provided may include:

- (a) Relevant legislation, regulatory information or industry norms;
- (b) Relevant (sectoral) studies or surveys (e.g. market surveys, technology studies, *etc*) undertaken by universities, research institutions, industry associations, companies, bilateral/multilateral institutions *etc*;
- (c) Relevant statistical data from national or international statistics;



- (d) Documentation of relevant market data (*e.g.* market prices, tariffs, rules);
- (e) Written documentation from the company or institution developing or implementing the CDM project activity or the CDM project developer, such as minutes from Board meetings, correspondence, feasibility studies, financial or budgetary information, *etc.*;
- (f) Documents prepared by the project developer, contractors or project partners in the context of the proposed project activity or similar previous project implementations;
- (g) Written documentation of independent expert judgments from industry, educational institutions (*e.g.* universities, technical schools, and training centers), industry associations and others.

***Sub-Step 3b: Show that the identified barriers would not prevent the implementation of at least one of the alternatives (except the proposed CDM project activity):***

- If any of the baseline scenario alternatives face barriers that would prohibit them from being implemented, then these should be eliminated;
- If all project alternatives are prevented by at least one barrier, either the proposed CDM project is itself the baseline or the set of project alternatives has to be completed to include the potential baseline;
- If there are several potential baseline scenario candidates, choose the most conservative alternative as a baseline scenario and go to Step 5, otherwise go to Step 4.

***Step 4: Identify the most economically attractive baseline scenario alternative:***

Determine which of the remaining project alternatives that are not prevented by any barrier is the most economically or financially attractive.

To conduct the investment analysis, use the following sub-steps:

***Sub-step 4a: Determine appropriate analysis method:***

Determine whether to apply a simple cost analysis or an investment comparison analysis. If all remaining project alternatives generate no financial or economic benefits other than CDM related income, then apply the simple cost analysis (Option 1). Otherwise, use the investment comparison analysis (Option 2).

***Sub-step 4b: Option 1: Apply simple cost analysis:***

Document the costs associated with alternatives to the CDM project activity and demonstrate that the corresponding activities produce no financial or economic benefits.

- If all alternatives do not generate any financial or economic benefits, then the least costly alternative among these alternative is pre-selected as the most plausible baseline scenario candidate;
- If one or more alternatives generate financial or economic benefits, then the simple cost analysis cannot be used to select the baseline scenario.

***Sub-step 4c: Option 2: Apply investment comparison analysis:***

Identify the financial indicator, such as IRR, NPV, cost benefit ratio, or unit cost of service most suitable for the project type and decision-making context.

Calculate the suitable financial indicator for each of the project alternatives that have not been eliminated in Step 3 and include all relevant costs (including, for example, the investment cost, the operations and maintenance costs, financial costs, *etc.*) and revenues (including subsidies/fiscal incentives, *etc.* where applicable), and, as appropriate, non-market costs and benefits in the case of public investors.



Present the investment analysis in a transparent manner and provide all the relevant assumptions in the CDM-PDD, so that a reader can reproduce the analysis and obtain the same results. Clearly present critical techno-economic parameters and assumptions (such as capital costs, fuel prices, lifetimes, and discount rate or cost of capital). Justify and/or cite assumptions in a manner that can be validated by the DOE. In calculating the financial indicator, the project's risks can be included through the cash flow pattern, subject to project-specific expectations and assumptions (e.g. insurance premiums can be used in the calculation to reflect specific risk equivalents).

Assumptions and input data for the investment analysis shall not differ across the project activity and its alternatives, unless differences can be well substantiated.

Present in the CDM-PDD submitted for validation a clear comparison of the financial indicator for the proposed project alternative.

The alternative that has the best indicator (e.g. highest IRR) can be pre-selected as the most plausible baseline scenario candidate.

#### ***Sub-step 4d: Sensitivity analysis (only applicable to Option 2)***

Include a sensitivity analysis that shows whether the conclusion regarding the financial attractiveness is robust to reasonable variations in the critical assumptions. The investment analysis provides a valid argument in selecting the baseline only if it consistently supports (for a realistic range of assumptions) the conclusion that the pre-selected baseline scenario candidate is likely to remain the most financially and/or economically attractive.

In case the sensitivity analysis is not fully conclusive, select the most conservative among the project alternatives that are the most financially and/or economically attractive according to both Steps 4c and the sensitivity analysis in the Step 4d, e.g., if the sensitivity analysis shows that one or more project alternatives compete with the one identified in Step 4c., select the alternative with the lowest GHG emissions.

#### **Additionality**

The additionality of the project activity shall be demonstrated and assessed using the latest version of the "Tool for the demonstration and assessment of additionality" agreed by the Executive Board, taking into account similarity of approaches used to determine baseline scenario and additionality.

Consistency shall be ensured between the identification of baseline scenario and the additionality demonstration. The baseline scenario alternative selected in the previous section shall be used as an alternative when applying the "Tool for the demonstration and assessment of additionality".

In case of a re-assessment of the baseline scenario as a consequence of new NO<sub>x</sub> regulations over the course of the crediting period of the proposed project activity, the re-assessment of baseline scenario shall be undertaken using the same procedure indicated above. In such a case, the additionality of the project must also be re-demonstrated.



## Baseline Emissions

Baseline emissions of year  $y$  (measured in t CO<sub>2</sub> eq.) are estimated for: (i) the Nitrous oxide destroyed in the project activity, which in the absence of project activity would have been released into the atmosphere; and (ii) steam generated in the project activity using waste heat of N<sub>2</sub>O destruction process, which in absence of the project activity would have been generated using fossil fuels. The Nitrous oxide eligible for crediting should be adjusted both for any increase in production over the crediting period and implementation of regulations on N<sub>2</sub>O emissions. The following equation estimates the baseline emissions:

$$BE_y = Q_{N_2O,y} \times GWP_{N_2O} + Q_{\text{Steam}_{p,y}} \times EF_{CO_2, \text{Steam},y} \quad (1)$$

Where:

- $Q_{N_2O,y}$  = Quantity of N<sub>2</sub>O destructed by the N<sub>2</sub>O destruction facility in the year  $y$
- $GWP_{N_2O}$  = Global warming potential of N<sub>2</sub>O, 310
- $Q_{\text{Steam}_{p,y}}$  = Quantity of steam generated by the N<sub>2</sub>O destruction facility in the year  $y$ , which in absence of the project activity would have been generated using fossil fuels
- $EF_{CO_2, \text{Steam},y}$  = CO<sub>2</sub> emission factor of steam

To determine the quantity of N<sub>2</sub>O destructed ( $Q_{N_2O,y}$ ) by the N<sub>2</sub>O destruction facility the minimum of the following two options shall be adopted.

### Option A: Based on the consumption of HNO<sub>3</sub>

$$Q_{N_2O,y} = P_{AdOH,y} \times EF_{N_2O,BI,y} \quad (2)$$

Where:

- $P_{AdOH,y}$  = Total amount of adipic acid produced credited for emission reduction in year  $y$  (tonnes)
- $EF_{N_2O,BI,y}$  = N<sub>2</sub>O emissions factor for adipic acid production (tN<sub>2</sub>O/t adipic acid). This is estimated as lower of the two: estimated as per Equation 4 below; and 0.27 t N<sub>2</sub>O per tonne of adipic acid produced as specified by the IPCC Good Practice Guidance

#### *Procedure for estimating $P_{AdOH,y}$*

To exclude possible increase in production of adipic acid during the crediting period and to avoid claiming of emission reductions from the increased capacity, the  $P_{AdOH,y}$  is capped to the highest value of historical production data during 3 years prior to the implementation of the project activity and the quantity of N<sub>2</sub>O estimated or measured shall be adjusted accordingly.

$$P_{AdOH,y} = \text{minimum} \{ P_{AdOH,pr,y}, P_{AdOH,bl} \} \quad (3)$$

Where:

- $P_{AdOH,pr,y}$  = Is the total amount of adipic acid produced in year  $y$  (tonnes)
- $P_{AdOH,bl}$  = Is the maximum value of total amount of adipic acid produced in most recent 3 years before the implementation of the project activity (tonnes)



*Procedure for estimating N<sub>2</sub>O emission factor*

EF<sub>N<sub>2</sub>O,Bl,y</sub> is estimated based on HNO<sub>3</sub> consumption and the assumption that by-products from nitric acid consumption are N<sub>2</sub>O and N<sub>2</sub> that are released with the reaction off-gases, as below:

$$EF_{N_2O,Bl,y} = \frac{Q_{HNO_3,cheml}}{P_{AdOH,y}} * \frac{63}{2} \times R_{N_2O-N_2,y} \times 44 \quad (4)$$

Where:

- Q<sub>HNO<sub>3</sub>,cheml</sub> = Total chemical consumption of HNO<sub>3</sub>, which is defined as total HNO<sub>3</sub> consumed less physical losses, as estimated using Equation 5 below
- R<sub>N<sub>2</sub>O-N<sub>2</sub>,y</sub> = The ratio of N<sub>2</sub>O to N<sub>2</sub> decomposed from the process for the year y

Project Participants may choose a conservative value for the ratio of N<sub>2</sub>O to N<sub>2</sub> depending on the feedstock. To obtain a conservative value for R<sub>N<sub>2</sub>O-N<sub>2</sub>,y</sub> the following method shall be used:

- Establish a table of R<sub>N<sub>2</sub>O-N<sub>2</sub></sub> in relation to the key factors such as ratio of cyclohexanone and cyclohexanol, drawing upon industry-approved or peer reviewed scientific information or validated in-house data, taking into account uncertainty;
- Establish a ceiling value of R<sub>N<sub>2</sub>O-N<sub>2</sub></sub> (R<sub>N<sub>2</sub>O-N<sub>2</sub>,max</sub>), based on the lowest annual average of the key factors affecting R<sub>N<sub>2</sub>O-N<sub>2</sub></sub> during the past three years;
- Establish an estimate of R<sub>N<sub>2</sub>O-N<sub>2</sub></sub> realtime (R<sub>N<sub>2</sub>O-N<sub>2</sub>,y</sub>), based on the key figures obtained during the implementation of project. R<sub>N<sub>2</sub>O-N<sub>2</sub>,y</sub> should not exceed R<sub>N<sub>2</sub>O-N<sub>2</sub>,max</sub>.

Total chemical consumption of HNO<sub>3</sub> shall be determined as follows:

$$Q_{HNO_3,Cheml} = Q_{HNO_3,cons,y} - (Q_{HNO_3,ww,y} + Q_{HNO_3,by-p,y} + Q_{HNO_3,AdOH,y} + Q_{NOX,offgases,y}) \quad (5)$$

Where:

- Q<sub>HNO<sub>3</sub>,cheml</sub> = Total chemical consumption of HNO<sub>3</sub>
- Q<sub>HNO<sub>3</sub>,cons,y</sub> = Consumption of HNO<sub>3</sub> in year y (tonnes)
- Q<sub>HNO<sub>3</sub>,ww,y</sub> = Quantity of nitrate in the waste water (tonnes). This is measured as product of nitrate concentration in waste water and waste water flow, measured on a daily basis
- Q<sub>HNO<sub>3</sub>,by-p,y</sub> = Quantity of nitrate in the by-products (tonnes). This is measured as product of nitrate concentration in by-products and by-products, measured on a regular interval
- Q<sub>HNO<sub>3</sub>,AdOH,y</sub> = Quantity of nitrate in the adipic acid produced (tonnes). This is measured as product of nitrate concentration in adipic acid and adipic acid production, measured on a regular interval
- Q<sub>HNO<sub>3</sub>,offgases,y</sub> = Quantity of nitrogen content in form NO<sub>x</sub> in the flue gases (tonnes). This is measured as product of NO<sub>x</sub> concentration in flue gases, quantity of flue gases and appropriate conversion factor from N in NO<sub>x</sub> to N in HNO<sub>3</sub>. The NO<sub>x</sub> measurement should be taken at a daily frequency

**Option B: Direct measurement of the quantity of N<sub>2</sub>O entering the destruction facility**

The actual quantity of N<sub>2</sub>O fed to the destruction facility shall be continuously monitored *ex post* during the crediting period. The measuring equipment shall be installed at the inlet of the N<sub>2</sub>O destruction facility. The measured value of N<sub>2</sub>O shall be adjusted for 5% uncertainty in measurements as follows:

$$Q_{N2O,y} = Q_{N2O,m,y} \times 0.95 \times f \quad (6)$$

Where:

- $Q_{N2O,y}$  = The quantity of N<sub>2</sub>O destructed during the year  $y$  in tonnes  
 $Q_{N2O,m,y}$  = Measured value of the quantity of N<sub>2</sub>O fed to the destruction facility in tonnes  
 $f$  = Correction factor for adipic acid production in year  $y$

$$f = \frac{P_{AdOH,y}}{P_{AdOH,Pr,y}} \quad (7)$$

Where,  $P_{AdOH,y}$  and  $P_{AdOF,Pr,y}$  are defined in Equation 3 above.

Procedure for Monitoring of N<sub>2</sub>O ( $Q_{N2O,m,y}$ )

To monitor the actual quantity of N<sub>2</sub>O fed to the decomposition facility, N<sub>2</sub>O concentration and gas volume flow are to be monitored on the same basis i.e. wet or dry. The monitoring system is to be installed using the European Norm 14181. This monitoring system provides separate readings for N<sub>2</sub>O concentration and gas flow volume for a defined period of time (e.g. every hour of operation, it provides an average of the measured values for the previous 60 minutes). Error readings (e.g. downtime or malfunction) and extreme values are to be automatically eliminated from the output data series by the monitoring system. Measurement results can be distorted before and after periods of downtime or malfunction of the monitoring system and can lead to mavericks. To eliminate such extremes and to ensure a conservative approach, the following statistical evaluation is to be applied to the complete data series of N<sub>2</sub>O concentration as well as to the data series for gas volume flow. The statistical procedure will be applied to data obtained after eliminating data measured for periods where the plant operated outside the plant's normal operating parameters:

- Calculate the sample mean ( $\bar{x}$ );
- Calculate the sample standard deviation ( $s$ );
- Calculate the 95% confidence interval (equal to 1.96 times the standard deviation);
- Eliminate all data that lie outside the 95% confidence interval;
- Calculate the new sample mean from the remaining values (volume of gas (VSG) and N<sub>2</sub>O concentration of gas (NCG)).

The average mass of N<sub>2</sub>O emissions per hour is estimated as product of the NCG and VSG. Total annual quantity of N<sub>2</sub>O can be determined as follows:

$$Q_{N2O,m,y} = \sum_h NCG_h \times VSG_h \times h_y \quad (8)$$



Where:

- $NCG_h$  = The  $N_2O$  concentration at the inlet of the destruction facility during the hour  $h$   
( $\text{ton } N_2O/\text{m}^3$ )<sup>3</sup>
- $VSG_h$  = The volume of gas flow at the inlet of the destruction facility during the hour  $h$  ( $\text{m}^3$ )
- $h_y$  = The number of hours of operation in a year  $y$

The above procedure shall be followed also for measuring the amount of  $N_2O$  that may be released to the atmosphere ( $Q_{N_2O, \text{by-pass}, y}$ ) and the amount of  $N_2O$  in exhaust of decomposition facility ( $Q_{ND\_N_2O, y}$ ), as defined in Equation 10 in project emission section.

#### Procedure for adjusting baseline $N_2O$ emissions for regulations

The quantity of  $N_2O$  determined shall be adjusted for mandatory regulations if exist/introduced in the Host country during the crediting period as follows:

If the regulation is based on the absolute quantity of  $N_2O$  emission permitted:

$$Q_{N_2O, y} = \text{minimum of } \{Q_{N_2O, y}, Q_{N_2O, \text{reg}}\} \quad (9)$$

Where,  $Q_{N_2O, \text{reg}}$  is absolute quantity of  $N_2O$  emission restriction and  $Q_{N_2O, y}$  is minimum of the two values estimated based on Option A and Option B described above.

If the regulation is an  $N_2O$  emissions rate:

$$Q_{N_2O, y} = \text{minimum} \{Q_{N_2O, y}, P_{AdOH, y} \times EF_{N_2O, \text{reg}}\} \quad (10)$$

Where,  $EF_{N_2O, \text{reg}}$  is the emission rate limit set by regulation,  $Q_{N_2O, y}$  is minimum of the two values estimated based on Option A and Option B described above, and  $P_{AdOH, y}$  is estimated using equation 3.

If the regulation is expressed as the share ( $r_y$ ) of the  $N_2O$  in the waste stream required to be destroyed:

$$Q_{N_2O, y} = Q_{N_2O, y} (1 - r_y) \quad (11)$$

Where  $Q_{N_2O, y}$  is minimum of the two values estimated based on Option A and Option B described above.

<sup>3</sup>  $VCG_h$  and  $NCG_h$  should be measured simultaneously, at same basis (wet or dry) and values should be expressed on the same basis (wet or dry) and should be corrected to normal conditions (101.325 kPa, 0 deg C). If the instrument (or measurement system) uses an algorithm to convert actual conditions to normal conditions, the proper source of such an algorithm should be used (e.g. based on procedures of EN14181). For all the cases, either manual or algorithm-based conversion of actual conditions to normal conditions, the temperature and pressure of actual conditions of gas should be recorded.

**Project emissions**

The emissions due to project activity in a year  $y$  ( $PE_y$ ) are determined as:

$$PE_y = PE_{N_2O,y} + PE_{FC,j,y} + PE_{EC,y} + PE_{NH_3,y} + PE_{HCE,y} \quad (12)$$

Where:

$PE_{N_2O,y}$  = Project  $N_2O$  emissions in year  $y$

$PE_{FC,j,y}$  = Project emissions from consumption of fossil fuel in the decomposition facility in year  $y$ . This includes hydro carbons used directly in the decomposition facility as well as fossil fuel used for generating steam or other form of energy that is used by the decomposition unit. Use the “Tool to calculate project or leakage  $CO_2$  emissions from fossil fuel combustion” to estimate this source of project emissions, where  $j$  are the process where fossil fuel is used in the decomposition process

$PE_{EC,y}$  = Project emissions from consumption of electricity in the decomposition facility in year  $y$ . Use the “Tool to calculate baseline, project and/or leakage emissions from electricity consumption” to estimate this source of project emissions

$PE_{NH_3,y}$  = Project emissions from use of Ammonia in DeNO<sub>x</sub> facility in year  $y$

$PE_{HCE,y}$  = Project emissions from use of hydro carbons in decomposition facility in year  $y$

$$PE_{N_2O,y} = (Q_{N_2O,by-pass,y} + Q_{ND\_N_2O,y}) \times GWP_{N_2O} \quad (13)$$

Where:

$Q_{N_2O,by-pass,y}$  = Project  $N_2O$  emissions from  $N_2O$  that is not sent to the decomposition facility in year  $y$

$Q_{ND\_N_2O,y}$  = Project  $N_2O$  emissions from  $N_2O$  released in effluent gases of decomposition facility in year  $y$

$$Q_{ND\_N_2O,y} = Q_{GE,y} \times C_{N_2O\_GE,y} \quad (14)$$

Where:

$Q_{GE,y}$  = The mass of effluent gas from decomposition facility (tonnes), in the year  $y$

$C_{N_2O\_GE,y}$  = The concentration of  $N_2O$  in effluent gas from decomposition facility (tonnes  $N_2O$ /tonne effluent gas) in year  $y$

$Q_{N_2O,by-pass,y}$  shall be directly monitored *ex post* during the crediting period. Otherwise project participants may monitor the time of opening the bypass line to enable gas venting into the atmosphere and account the bypass quantity as follows:

$$Q_{N_2O,by-pass,y} = Q_{N_2O,m,y} \times T_{open,y} \quad (15)$$

Where:

$Q_{N_2O,m,y}$  = Measured value of the quantity of  $N_2O$  fed to the destruction facility in tonnes in year  $y$

$T_{open,y}$  = % of time the valve on the line feeding the decomposition facility is open in year  $y$  to release the gas directly into the atmosphere

PE<sub>NH3</sub>: Ammonia input to the destruction facility:

- In case a SCR DeNO<sub>x</sub> unit is already installed prior to the starting date of the project activity or has to be installed according to legal requirements, the project ammonia input will be considered equal to the ammonia input of the baseline scenario;
- Should no SCR DeNO<sub>x</sub> unit be installed prior to the starting date of the project activity, project emissions related to the production of ammonia are considered as follows:

$$PE_{NH_3,y} = Q_{NH_3,y} \times EF_{NH_3} \quad (16)$$

Where:

- $PE_{NH_3,y}$  = Project emissions related to ammonia input to destruction facility in year  $y$  (tCO<sub>2</sub>e)  
 $Q_{NH_3,y}$  = Ammonia input to the destruction facility in year  $y$  (tNH<sub>3</sub>)  
 $EF_{NH_3}$  = GHG emissions factor for ammonia production (CO<sub>2</sub>e/tNH<sub>3</sub>), a default factor of 2.14 tCO<sub>2</sub>e/tNH<sub>3</sub> is suggested (GEMIS 4.2)

Project emissions are limited to the existing production capacity (maximum of 3 years historical production data prior to the implementation of the project activity) of the existing adipic acid production plant. If the actual production ( $P_{AdOH,y}$ ) exceeds the existing capacity then emissions related to the production above existing capacity will neither be claimed for the baseline nor for the project scenario.

**Leakage**

Leak emissions comprise the emissions associated with the energy sources used to generate any steam used by the decomposition plant, where the steam is produced outside the project boundary. When the steam is produced within the project boundary, these emissions are captured as project emissions from consumption of fossil fuels.

Leakage amounts to:

$$L_y = Q_{St,c,y} \times EF_{St,c,y} \quad (17)$$

Where:

- $Q_{St,c,y}$  = The steam consumption of the facility (TJ)  
 $EF_{St,c,y}$  = The CO<sub>2</sub> emission factor of the steam generation, tCO<sub>2</sub>/TJ and is taken as the emission factor of the plant from which the steam is purchased

**Emission Reductions**

The greenhouse gas emission reduction (ER<sub>y</sub>) achieved by the project activity in a year  $y$  is the baseline emissions of the adipic acid plant less the greenhouse gas emissions generated by the decomposition process (PE<sub>y</sub>) less leakage due to the decomposition process (L<sub>y</sub>).

$$ER_y = BE_y - PE_y - L_y \quad (18)$$

**Changes required for methodology implementation in 2nd and 3rd crediting periods**

- If new or modified NO<sub>x</sub> emission regulations are introduced after the project start, determination of the baseline scenario will be re-assessed at the renewal of the crediting period.

For the determination of the adjusted baseline scenario the project participant should re-assess the baseline scenario and shall apply baseline determination process as stipulated above (Steps 1 – 4).

Potential outcomes of the re-assessment of the Baseline Scenario (to be in line with NO <sub>x</sub> regulation)	Consequence (adjusted baseline scenario)
SCR De NO <sub>x</sub> installation	Continuation of original (N <sub>2</sub> O) baseline scenario
NSCR De NO <sub>x</sub> installation	The N <sub>2</sub> O emissions outlet of NSCR become adjusted baseline N <sub>2</sub> O emissions, as NSCR may reduce N <sub>2</sub> O emissions as well as NO <sub>x</sub>
Tertiary measure that combines NO <sub>x</sub> and N <sub>2</sub> O emission reduction	Adjusted baseline scenario results in zero N <sub>2</sub> O emissions reduction
Continuation of original baseline scenario	Continuation of original baseline scenario

**Data and parameters not monitored**

<b>Data / parameter:</b>	GWP <sub>N<sub>2</sub>O</sub>
Data unit:	tCO <sub>2</sub> e/tN <sub>2</sub> O
Description:	Global warming potential of the N <sub>2</sub> O during the crediting period
Source of data:	IPCC
Measurement procedures (if any):	
Any comment:	Default value 310, to be checked at the renewal of crediting period

<b>Data / parameter:</b>	EF <sub>NH<sub>3</sub></sub>
Data unit:	Tonnes N <sub>2</sub> O/tonnes NH <sub>3</sub>
Description:	Emission factor of N <sub>2</sub> O per per tonne of NH <sub>3</sub> used
Source of data:	GEMIS 4.2
Measurement procedures (if any):	
Any comment:	Default value 2.14



<b>Data / parameter:</b>	$P_{AdOH, BL}$
Data unit:	Tonnes of AdOH
Description:	Maximum value of total amount of adipic acid produced in most recent 3 years before the implementation of the project activity
Source of data:	Measured
Measurement procedures (if any):	
Any comment:	For the cases, where adipic acid production cannot be measured directly, refer to the procedure under Annex 1 on “Procedure to estimate adipic acid production in cases it cannot be measured directly” .

<b>Data / parameter:</b>	$NCG_h$
Data unit:	ton $N_2O/m^3$ at normal conditions
Description:	$N_2O$ concentration at the inlet of the destruction facility during the hour $h$
Source of data:	Measured
Measurement procedures (if any):	
Monitoring frequency:	Continuous
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project’s lifetime

<b>Data / parameter:</b>	$VSG_h$ at normal conditions
Data unit:	$m^3$
Description:	Volume of gas flow at the inlet of the destruction facility during the hour $h$
Source of data:	Measured
Measurement procedures (if any):	
Monitoring frequency:	Continuous
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project’s lifetime

<b>Data / parameter:</b>	$h_y$
Data unit:	-
Description:	Number of hours of operation in a year $y$
Source of data:	Measured
Measurement procedures (if any):	
Monitoring frequency:	Monthly
QA/QC procedures:	
Any comment:	Records to be maintained during project’s lifetime



<b>Data / parameter:</b>	$P_{AdOH,pr,y}$
Data unit:	Tonnes of AdOH
Description:	Quantity of Adipic acid produced during the year $y$
Source of data:	Measured
Measurement procedures (if any):	
Monitoring frequency:	Monthly
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime. For the cases, where adipic acid production cannot be measured directly, refer to the procedure under Annex-1 on "Procedure to estimate adipic acid production in cases it cannot be measured directly".

<b>Data / parameter:</b>	$Q_{HNO_3,cons,y}$
Data unit:	Tonnes
Description:	Quantity of $HNO_3$ consumption during the year $y$
Source of data:	Measured
Measurement procedures (if any):	
Monitoring frequency:	Monthly
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$Q_{HNO_3,ww,y}$
Data unit:	Tonnes
Description:	Quantity of $HNO_3$ loss in waste water during the year $y$
Source of data:	Measured
Measurement procedures (if any):	This is measured as product of nitrate concentration in waste water and waste water flow
Monitoring frequency:	Daily
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$Q_{HNO_3,by-p,y}$
Data unit:	Tonnes
Description:	Quantity of $HNO_3$ in byproducts, during the year $y$
Source of data:	Measured
Measurement procedures (if any):	
Monitoring frequency:	Monthly
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime





<b>Data / parameter:</b>	$Q_{\text{HNO}_3, \text{AdOH}, y}$
Data unit:	Tonnes
Description:	Quantity of $\text{HNO}_3$ in adipic acid produced during the year $y$
Source of data:	Measured
Measurement procedures (if any):	This is measured as product of nitrate concentration in adipic acid and adipic acid produced.
Monitoring frequency:	Monthly
QA/QC procedures:	Measuring instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$Q_{\text{NO}_x, \text{offgases}, y}$
Data unit:	Tonnes
Description:	Quantity of nitrogen content in off gases during the year $y$
Source of data:	Measured
Measurement procedures (if any):	This is measured as product of $\text{NO}_x$ concentration in flue gases, flow of gas, appropriate conversion factor from N in $\text{NO}_x$ to N in $\text{HNO}_3$ .
Monitoring frequency:	Daily
QA/QC procedures:	Measuring instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$R_{\text{N}_2\text{O}-\text{N}_2, y}$
Data unit:	
Description:	Ratio of $\text{N}_2\text{O}$ to $\text{N}_2$
Source of data:	Measured/Calculated
Measurement procedures (if any):	To obtain figures for $R_{\text{N}_2\text{O}-\text{N}_2, y}$ the following methods must be selected: <ul style="list-style-type: none"> <li>Establish a table of <math>R_{\text{N}_2\text{O}-\text{N}_2}</math> in relation to the key factors such as ratio of cyclohexanone and cyclohexanol, drawing upon industry-approved or peer reviewed scientific information or validated in-house data, taking into account uncertainty;</li> <li>Establish a ceiling value of <math>R_{\text{N}_2\text{O}-\text{N}_2}</math> (<math>R_{\text{N}_2\text{O}-\text{N}_2, \text{max}}</math>), based on the lowest annual average of the key factors affecting <math>R_{\text{N}_2\text{O}-\text{N}_2}</math> during the past three years';</li> <li>Establish an estimate of <math>R_{\text{N}_2\text{O}-\text{N}_2}</math> realtime (<math>R_{\text{N}_2\text{O}-\text{N}_2, y}</math>), based on the key figures obtained during the implementation of project. <math>R_{\text{N}_2\text{O}-\text{N}_2, y}</math> should not exceed <math>R_{\text{N}_2\text{O}-\text{N}_2, \text{max}}</math>.</li> </ul>
Monitoring frequency:	Daily
QA/QC procedures:	Measuring instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$Q_{\text{N}_2\text{O}, \text{reg}}$
Data unit:	Tonnes
Description:	Quantity of $\text{N}_2\text{O}$ allowed under regulations
Source of data:	Regulation
Measurement procedures (if any):	Depends on regulation.
Monitoring frequency:	At date of introduction or change of regulation
QA/QC procedures:	
Any comment:	Records to be maintained during project's lifetime



<b>Data / parameter:</b>	$EF_{N_2O,reg}$
Data unit:	Tonnes N <sub>2</sub> O/tonnes AdOH
Description:	Quantity of N <sub>2</sub> O allowed under regulations per tonne of AdOH produced
Source of data:	Regulation
Measurement procedures (if any):	Depends on regulation.
Monitoring frequency:	At date of introduction or change of regulation
QA/QC procedures:	
Any comment:	Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$r_v$
Data unit:	
Description:	% of N <sub>2</sub> O allowed under regulations
Source of data:	Regulation
Measurement procedures (if any):	Depends on regulation.
Monitoring frequency:	At date of introduction or change of regulation
QA/QC procedures:	
Any comment:	Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$Q_{Steam,p,y}$
Data unit:	TJ/hr.
Description:	Steam production by the decomposition process
Source of data:	Measured
Measurement procedures (if any):	Measured as energy value by means of pressure, temperature and flow of steam
Monitoring frequency:	Continuous
QA/QC procedures:	Shall be measured using steam flow meter
Any comment:	Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$EF_{CO_2,Steam,v}$
Data unit:	tCO <sub>2</sub> /t-steam
Description:	CO <sub>2</sub> intensity for steam <sup>4</sup>
Source of data:	Calculated
Measurement procedures (if any):	
Monitoring frequency:	Yearly
QA/QC procedures:	
Any comment:	Records to be maintained during project's lifetime

<sup>4</sup> This CO<sub>2</sub> intensity is related to the steam produced by the existing supplier and that will be produced by the project.



<b>Data / parameter:</b>	$Q_{St, c, y}$
Data unit:	TJ/hr.
Description:	Steam consumption by the decomposition process
Source of data:	Measured
Measurement procedures (if any):	Measured as energy value by means of pressure, temperature and flow of steam
Monitoring frequency:	Continuous
QA/QC procedures:	Shall be measured using steam flow meter
Any comment:	This parameter is applicable only when the destruction facility uses steam supplied by others. Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$EF_{St, c, y}$
Data unit:	tCO <sub>2</sub> /t-steam
Description:	CO <sub>2</sub> intensity for steam <sup>5</sup>
Source of data:	Calculated
Measurement procedures (if any):	Calculated from the steam supplier data
Monitoring frequency:	Yearly
QA/QC procedures:	
Any comment:	Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$Q_{N_2O, bypass, y}$
Data unit:	Tonnes of N <sub>2</sub> O
Description:	Quantity of N <sub>2</sub> O bypassed during the year <i>y</i>
Source of data:	Measured
Measurement procedures (if any):	To monitor the actual quantity of N <sub>2</sub> O, both N <sub>2</sub> O concentration and gas volume flow are to be measured. The product of N <sub>2</sub> O concentration and flow is the actual N <sub>2</sub> O fed to the decomposition facility. The monitoring system shall comply with the European Norm 14181. Further details are provided in the baseline methodology procedure.
Monitoring frequency:	Continuous
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime

<b>Data / parameter:</b>	$Q_{GE, y}$
Data unit:	Tonnes
Description:	Quantity of effluent gas generated during the year <i>y</i>
Source of data:	Measured
Measurement procedures (if any):	
Monitoring frequency:	Continuous
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime. The monitoring system shall comply with the European Norm 14181. Further details are provided in the baseline methodology procedure.

<sup>5</sup> This CO<sub>2</sub> intensity is related to the steam produced by the existing supplier and that will be produced by the project.



<b>Data / parameter:</b>	$C_{N_2O,GE,y}$
Data unit:	Tonnes of $N_2O$ /tonne of effluent gas
Description:	$N_2O$ concentration in the effluent gas
Source of data:	Measured
Measurement procedures (if any):	
Monitoring frequency:	Monthly
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime. The monitoring system shall comply with the European Norm 14181. Further details are provided in the baseline methodology procedure.

<b>Data / parameter:</b>	$T_{Open,y}$
Data unit:	%
Description:	% of time the valve on the line feeding the decomposition facility is open in year $y$
Source of data:	Measured
Measurement procedures (if any):	Measured as a percentage by monitoring the period of opened condition and the total operating hours of the production facility
Monitoring frequency:	Yearly
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project's lifetime. This parameter is used when $Q_{N_2O,bypass,y}$ is not directly monitored

<b>Data / parameter:</b>	$PE_{FC,i,y}$
Data unit:	tCO <sub>2e</sub>
Description:	Project emissions from consumption of fossil fuel in the decomposition facility in year $y$
Source of data:	Calculated as per the "Tool to calculate project or leakage CO <sub>2</sub> emissions from fossil fuel combustion"
Measurement procedures (if any):	As per the "Tool to calculate project or leakage CO <sub>2</sub> emissions from fossil fuel combustion"
Monitoring frequency:	As per the "Tool to calculate project or leakage CO <sub>2</sub> emissions from fossil fuel combustion"
QA/QC procedures:	As per the "Tool to calculate project or leakage CO <sub>2</sub> emissions from fossil fuel combustion"
Any comment:	-



<b>Data / parameter:</b>	$PE_{EC,y}$
Data unit:	tCO <sub>2</sub>
Description:	Project emissions from consumption of electricity in the decomposition facility in year $y$
Source of data:	Calculated as per the “Tool to calculate baseline, project and/or leakage emissions from electricity consumption”
Measurement procedures (if any):	As per the “Tool to calculate baseline, project and/or leakage emissions from electricity consumption”
Monitoring frequency:	As per the “Tool to calculate baseline, project and/or leakage emissions from electricity consumption”
QA/QC procedures:	As per the “Tool to calculate baseline, project and/or leakage emissions from electricity consumption”
Any comment:	-

<b>Data / parameter:</b>	$Q_{NH_3,y}$
Data unit:	tNH <sub>3</sub>
Description:	Ammonia input to the destruction facility in year $y$
Source of data:	Measured
Measurement procedures (if any):	
Monitoring frequency:	Continuous
QA/QC procedures:	Metering instruments shall be calibrated regularly to industry standards
Any comment:	Records to be maintained during project’s lifetime

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**Annex 1****Procedure to estimate adipic acid production in cases it cannot be measured directly<sup>6</sup>**

In order to apply this procedure to their project activity, the project proponents are required to demonstrate the following.

- It should be demonstrated that direct measurement of adipic acid is not possible due to factors such as facility design; and
- It should be demonstrated that it is not possible to consume adipic acid sourced from outside in the production process concerned, for the purpose of producing derivatives of adipic acid.

For facilities where production of adipic acid ( $P_{AdOH}$ ) cannot be obtained by measurement as specified in this methodology, it can be estimated through a stoichiometric calculation from derivative of AdOH, through the following equation;

$$P_{AdOH} = (146.14/MW_x) * P_x$$

Where:

$P_x$  = Total amount of derivative of AdOH (substance x) produced credited for emission reduction in year y (tonnes)

$MW_x$  = Molecular weight of substance x which is the derivative of adipic acid (AdOH) (g/mole)

146.14 = Molecular weight of adipic acid.

An example of substance eligible for *substance x* is AHS, then  $MW_x$  is 262.14:

In the case of nylon 66 salt (AHS) production, its quantity is estimated as the product of nylon 66 salt concentration in aqueous solution of nylon 66 salt and mass of aqueous solution of nylon 66 salt production). Further revision from the methodology AM0021 may be proposed for the production of other substances (e.g. finished product of nylon 66), in case this guidance cannot be applied to the production of these substances.

<sup>6</sup> There is a separate EB guidance “Guidance to estimate adipic acid production in cases where it cannot be measured directly” which makes this procedure applicable to all the versions of AM0021.



## History of the document

Version	Date	Nature of revision(s)
03	EB 45, Annex # 13 February 2009	Revision includes the procedure in Annex 1 to estimate the adipic acid production in cases it cannot be measured directly.
02.2	EB 41, Annex 7 02 August 2008	Editorial revision to add footnote 3 to clarify that volume of gas and N <sub>2</sub> O concentration should be measured simultaneously and at same basis (wet or dry) and should be expressed at the normal conditions. The clarification made in the monitoring tables of these parameters also.
02.1	EB 39, Paragraph 22 16 May 2008	“Tool to calculate baseline, project and/or leakage emissions from electricity consumption” replaces the withdrawn “Tool to calculate project emissions from electricity consumption”.
02	EB 36, Annex 8 30 November 2007	Revision to include the following <ul style="list-style-type: none"><li>• Clear procedures for the identification of the baseline scenario;</li><li>• Clearer procedures for estimating the baseline N<sub>2</sub>O emission using equations;</li><li>• A requirement to measure the N<sub>2</sub>O emissions before the destruction unit to estimate the baseline N<sub>2</sub>O emissions;</li><li>• Further clarity in the monitoring requirements.</li></ul>
01	EB 18, Annex 2 25 February 2005	Initial adoption.