

**Draft revision to approved baseline methodology AM0001****“Incineration of HFC 23 waste streams”****Source**

This methodology is based on a proposal from the HFC Decomposition Project in Ulsan, Republic of Korea whose Baseline study, Monitoring and Verification Plan and Project Design Document were prepared by INEOS Fluor Japan Limited (Japan), Foosung Tech Corporation Co., Ltd. (Korea) and UPC Corporation Ltd. (Korea) (version 2.4, July 8, 2003). For more information regarding the proposal and its consideration by the Executive Board please refer to case NM007: “HFC Decomposition Project in Ulsan” on

<http://cdm.unfccc.int/methodologies/PAmethodologies/approved.html>

Selected approach from paragraph 48 of the CDM modalities and procedures

“Existing actual or historical emissions, as applicable”

Applicability

This methodology is applicable to HFC 23 (CHF_3) waste streams from an existing HCFC22 production facility with at least three (3) years of operating history between beginning of the year 2000 and the end of the year 2004 where the project activity occurs and where no regulation requires the destruction of the total amount of HFC23 waste.

This baseline methodology shall be used in conjunction with the approved monitoring methodology AM0001/version 3 (“Incineration of HFC 23 waste streams”).

Project Activity

Production of HCFC 22 generates the HFC 23. Some of the HFC 23 may be captured and sold, but the HFC 23 may also be released to the atmosphere. The project activity captures and decomposes the HFC 23 that would otherwise be released to the atmosphere (and any HCFC 22 present in this waste stream)¹.

¹ In the example of the Ulsan project activity proposal the destruction process will decompose the HFC 23 by heating it to more than 1,200°C in a thermal oxidation chamber with air and steam using LNG as a supplemental fuel. This yields CO₂, HCl and HF as by-products in a hot stream of offgas that also contains nitrogen, oxygen, carbon dioxide and moisture. This gas stream is cooled, the acids and moisture are absorbed in an aqueous solution and the acids in the solution are then neutralized with slaked lime to yield calcium chloride (CaCl₂) and calcium fluoride (CaF₂). The CaCl₂ and CaF₂ are disposed in a landfill. The remaining cooled and neutralised gas (now nitrogen/oxygen/carbon dioxide with low levels of moisture) is vented to atmosphere.



Emission Reduction

Waste HFC 23 is typically released into the atmosphere. Thus, absent regulations to restrict HFC 23 emissions, any HFC 23 not recovered for sale is assumed to be released to the atmosphere.

The greenhouse gas emission reduction achieved by the project activity is the quantity of waste HFC 23 actually destroyed less the greenhouse gas emissions generated by the destruction process less leakage due to the destruction process. Specifically, the greenhouse gas emission reduction (ER_y) achieved by the project activity during a given year (y) is equal to the quantity of HFC 23 waste from HCFC production facility (Q_HFC23_y) destroyed by the project activity less the baseline HFC 23 destruction (B_HFC23_y) during that year multiplied by the approved Global Warming Potential² value for HFC23 (GWP_HFC23) less the greenhouse gas emissions generated by the destruction process (E_DP_y) less greenhouse gas leakage (L_y) due to the destruction process.

$$ER_y = (Q_HFC23_y - B_HFC23_y) * GWP_HFC23 - E_DP_y - L_y \quad (1)$$

Where ER_y is the greenhouse gas emission reduction measured in tonnes of CO₂ equivalents (tonnes CO₂e), Q_HFC23_y is the quantity of waste HFC 23 destroyed during the year measured metric tonnes, and B_HFC23_y is the baseline quantity of HFC 23 destroyed during the year measured in metric tonnes. The Global Warming Potential converts 1 tonne of HFC 23 to tonnes of CO₂ equivalents (tonnes CO₂e/tonnes HFC 23). The approved Global Warming Potential value for HFC 23 is 11,700 tonnes CO₂e/tonne HFC 23. The emissions due to the destruction process (E_DP_y) and leakage (L_y) are both measured in tonnes of CO₂ equivalent. The quantity of waste HFC 23 destroyed (Q_HFC23_y) is calculated as the product of the quantity of waste HFC 23 supplied to the destruction process (q_HFC23_y) measured in metric tonnes and the purity of the waste HFC 23 (P_HFC23_y) supplied to the destruction process expressed as the fraction of HFC 23 in the waste [$Q_HFC23_y = q_HFC23_y * P_HFC23_y$].

The destruction process uses fuel (e.g., natural gas), steam and/or electricity. The steam and electricity are assumed to be purchased, so the emissions associated with these energy sources are included in the leakage calculation.³ The emissions due to the destruction process (E_DP_y) are the emissions due to the natural gas use, the emissions of HFC 23 not destroyed and the greenhouse gas emissions of the destruction process. Thus:

$$E_DP_y = ND_HFC23_y * GWP_HFC23 + Q_NG_y * E_NG_y + Q_HFC23_y * EF \quad (2)$$

Where ND_HFC23_y is the quantity of HFC 23 not destroyed during the year, Q_NG_y is the quantity of natural gas used by the destruction process during the year measured in cubic-metres (m³), and E_NG_y is the emissions coefficient for natural gas combustion measured in tonnes CO₂ equivalent per cubic metre of natural gas (t CO₂e/m³). The value of E_NG_y will vary by region and over time⁴, but is of the order of 0.00188 tCO₂e/m³. If a different fuel, such as liquid petroleum gas (LPG), is used for the

² Global Warming Potential values used shall be those provided by the Intergovernmental Panel on Climate Change in its Second Assessment Report (“1995 IPCC GWP values”).

³ If the steam and/or electricity was generated within the project boundary, the associated emissions would be included in the equation for the emissions due to the destruction process.

⁴ In the example of the proposed Ulsan project activity it is of the order of 0.00188 tCO₂e/m³.



incineration process, the variables Q_{NG_y} and E_{NG_y} are replaced with variables for the quantity of fuel used and emissions coefficient for that fuel.

The quantity of HFC 23 not destroyed (ND_{HFC23_y}) is typically small⁵; the monitoring plan provides for its periodic on site measurement. Theoretically HFC 23 can also leak to the water effluent and then escape to the atmosphere. This possibility is ignored because it is infinitesimally small; the solubility of HFC 23 is 0.1% wt at 25°C water.

The thermal destruction process converts the carbon in the HFC 23 into CO_2 , which is released to the atmosphere. The quantity of CO_2 produced by the destruction process is the product of the quantity of waste HFC 23 (Q_{HFC23_y}) destroyed and the emission factor (EF). The emission factor is calculated as follows:

$$EF = 44 / [(\text{molecular weight of HFC 23}) / (\text{number of C in a molecule of HFC 23})] = 44 / [70 / 1] = 0.62857 \quad (3)$$

The thermal destruction process also produces a small quantity of N_2O emissions. The N_2O emissions, on a CO_2 equivalent basis, are a small fraction of the CO_2e emissions and so are ignored.

Baseline

The baseline quantity of HFC 23 destroyed is the quantity of the HFC 23 waste stream required to be destroyed by the applicable regulations. If the entire waste stream is destroyed, Q_{HFC23_y} is the total amount of HFC 23 waste generated and the quantity required to be destroyed by the applicable regulations is:

$$B_{HFC23_y} = Q_{HFC23_y} * r_y \quad (4)$$

Where r_y is the fraction of the waste stream required to be destroyed by the regulations that apply during year y . In the absence of regulations requiring the destruction of HFC 23 waste, the typical situation in non-Annex B Parties, $r_y = 0$. Absent regulations on HFC 23 emissions, the HFC 23 waste is typically released to the atmosphere so the baseline is zero destruction. **If the local regulation is modified during the crediting period, the possible impact on the calculation of baseline emissions shall be considered without delay by adapting the baseline HFC23 destruction rate.**

To exclude the possibility of manipulating the production process to increase the quantity of waste, the quantity of HFC 23 waste (Q_{HFC23_y}) is limited to a fraction (w) of the actual HCFC production during the year at the originating plant (Q_{HCFC_y}).

$$Q_{HFC23_y} \leq Q_{HCFC_y} * w \quad (5)$$

Where Q_{HCFC_y} is the actual production of HCFCs during the year at the plant where the HFC 23 waste originates measured in metric tonnes. **Q_{HCFC_y} is limited to the maximum historical annual production level at this plant (in tonnes of HCFC22) during any of the last three (3) years between**

⁵ In the example of the proposed Ulsan project activity the quantity of HFC 23 not destroyed is estimated at 0.001% of the quantity of HFC 23 supplied to the destruction process.



beginning of the year 2000 and the end of the year 2004, including CFC production at swing plants adjusted appropriately to account for the different production rates of HCFC22 and CFCs.

The coefficient w is the waste generation rate (HFC 23⁶)/(HCFC 22) for the originating plant. The historical waste generation shall be estimated for the three (3) most recent years of operation up to 2004. Direct measurement of HFC23 release is to be used where data are available, otherwise mass balance or other methods based on actual data⁷ (add footnote) are to be used. Uncertainty in emission rate estimates shall be quantified and conservative emission rate estimates shall be used when calculating expected emission reductions.

The value of w is set at the lowest of the three historical annual values estimated as specified above and is not to exceed 3% (0.03 tonnes of HFC 23 produced per tonne of HCFC 22 manufactured).

If insufficient data is available for the calculation of HFC23 release for all three (3) most recent years of operation up to 2004, then the default value for w to be used is 1.5%.

Additionality

In the absence of regulations requiring HFC 23 destruction it is typically released to the atmosphere because a destruction facility entails significant capital and operating costs and the host entity has no direct economic incentive to incur these costs. If the quantity of HFC 23 destroyed is greater than the baseline quantity destroyed, the project activity is additional. The baseline quantity of HFC 23 destroyed is the quantity, if any, required to be destroyed by the host country's regulations governing the plant.

Leakage

Leakage is emissions of greenhouse gases due to the project activity that occur outside the project boundary. The sources of leakage due to the destruction process are:

- Greenhouse gas (CO₂ and N₂O) emissions associated with the production of purchased energy (steam and/or electricity)
- CO₂ emissions due to transport of sludge to the landfill

$$L_y = \sum_i (Q_{F_{i,y}} * E_{F_{i,y}}) + ET_y \quad (6)$$

Where $Q_{F_{i,y}}$ is the quantity of energy type F_i purchased for the destruction process during year y , $E_{F_{i,y}}$ is the greenhouse gas emissions factor for energy type F_i during year y , and ET_y and the greenhouse gas emissions associated with sludge transport during year y .

⁶ The quantity of HFC 23 used to calculate this coefficient is the sum of HFC 23 recovered for sale plus the waste HFC 23.

⁷ The estimation may be based on the carbon efficiency and the fluorine efficiency of the process and normally the average of the two values shall be used unless there are overriding considerations (such as a much lower uncertainty of one of the two evaluations) that can be adequately documented. If HCFC22 leakage was not directly measured, the carbon and fluorine efficiencies may be used to determine both HFC23 waste and HCFC22 leakage. The DOE shall verify if the estimates obtained in this way can reasonably be used to calculate w or if it shall be considered that insufficient data are available to calculate HFC23 release for this plant (and therefore require the use of a default value of 1.5%).



Draft revision to approved monitoring methodology AM0001

“Incineration of HFC 23 waste streams”

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Applicability

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This monitoring methodology shall be used in conjunction with the approved baseline methodology AM0001/version 3 (“Incineration of HFC 23 waste streams”).

Monitoring Methodology

Monitoring methodology is based on direct measurement of the amount of HFC 23 waste destroyed and of the energy used by the destruction process as shown in Figure 1.

This monitoring methodology provides for direct and continuous measurement of the actual quantity HFC 23 destroyed, as well as the quantities of electricity, steam and fossil fuel used by the destruction process.

The emission reductions are dominated by the quantity of HFC 23 destroyed. To measure this quantity accurately two flow meters, each of which is recalibrated weekly, are used. Most of the time, under normal operation, both flow meters measure the same amount of HFC 23 flows simultaneously. Where the flowmeter readings differ by greater than twice their claimed accuracy (for example 10% if the accuracy is claimed to be $\pm 5\%$) then the reason for the discrepancy is investigated and the fault remedied. For the sake of conservativeness the lower value of the two readings will always be used to estimate the HFC 23 waste flows.

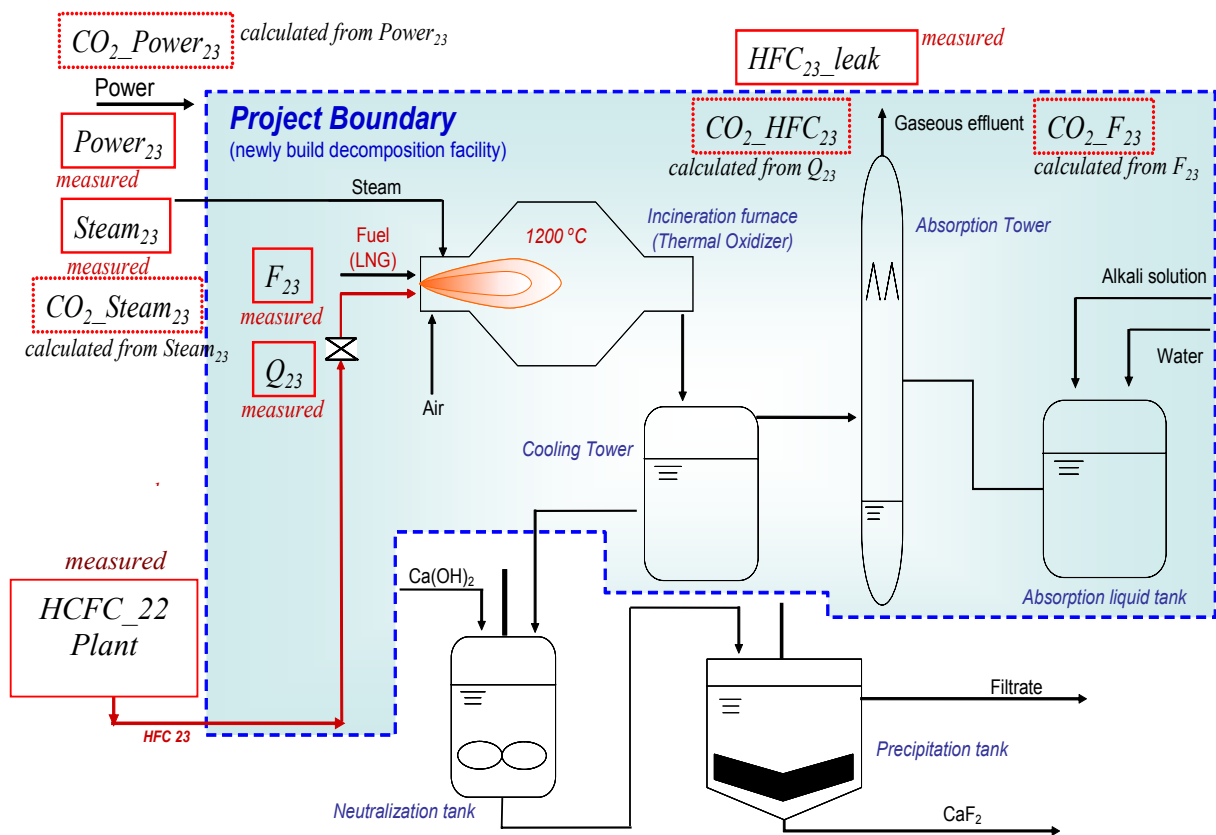
Other factors in the monitoring process for quality control are:

- Purity of HFC 23 is checked monthly by sampling using gas chromatography. Combinations of continuous flow measurement and calculation will be used to estimate quantities of other materials, e.g., air that may be in the HFCs if this is appropriate.
- Amount of HFC 23 waste generated. The output of HFC 23 from the HCFC 22 plant will be checked yearly by comparing the amount of HCFC 22 produced to the sum of the HFC 23 recovered for sale and HFC 23 decomposed.

The quantities of gaseous effluents (CO, HCl, HF, Cl₂, dioxin and NO_x) and liquid effluents (PH, COD, BOD, n-H (normal hexane extracts), SS (suspended solid), phenol, and metals (Cu, Zn, Mn and Cr) are measured every six months to ensure compliance with environmental regulations.

The monitoring methodology also requires the examination of local regulations regarding HFC₂₃ destruction on a yearly basis. If the local regulation is modified, the possible impact on the calculation of baseline emissions shall be considered without delay as specified in the baseline methodology.

Figure 1
Monitoring Plan



$$\begin{aligned}
 CO_{2_Power23} &= E_{F1,y} \\
 Power_{23} &= Q_{F1,y} \\
 Steam_{23} &= Q_{F2,y} \\
 CO_{2_Steam23} &= E_{F2,y} \\
 HCFC_{22\ Plant} &= Q_{HCFC_y} \\
 F_{23} &= Q_{NG_y} \\
 CO_{2_F23} &= Q_{NG_y} * E_{NG_y} \\
 Q_{23} &= Q_{HFC23_y} \\
 HFC_{23_leak} &= ND_{HFC23_y} \\
 CO_{2_HFC23} &= Q_{HFC23_y} * EF
 \end{aligned}$$

**Data to be collected or used to monitor emissions from the project activity, and how this data will be archived**
Monitored data for project emissions in the boundary (GHG)

ID number	Data type	Data variable	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/paper)	For how long is archived data kept?	Comment
1. q_HFC23y	Mass	Quantity of HFC 23 supplied to the destruction process	kg-HFC	(m) measured by flow meters in parallel that are calibrated weekly	monthly	100%	electronic	Project lifetime	
2. HFC23y	%	Purity of the HFC 23 supplied to the destruction process	%	(m) measured monthly by sampling	monthly		electronic	Project lifetime	Measured using gas chromatography
3. Q_NGy	Mass	Quantity of natural gas used by the destruction process	m ³	(m) measured	monthly	100%	electronic	Project lifetime	Measured using a fuel meter

In addition the quantities of gaseous effluents (CO, HCl, HF, Cl₂, dioxin and NOX) and liquid effluents (PH, COD, BOD, n-H (normal hexane extracts), SS (suspended solid), phenol, and metals (Cu, Zn, Mn and Cr) are measured in a manner and with a frequency that complies with local environmental regulations.



D.4. 1 Potential sources of emissions which are significant and reasonably attributable to the project activity, but which are not included in the project boundary, and identification if and how data will be collected and archived on these emission sources.

Monitored data for project emissions outside of the boundary (GHG)

ID number	Data type	Data variable	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/paper)	For how long is archived data kept?	Comment
4. ND_HFC23y	Mass	Quantity of HFC 23 in gaseous effluent	kg-HFC	(m) measured	monthly	100%	electronic	Project lifetime	When the thermal oxidizer stops, analysis of the effluent gas is done to check leaked HFC 23 by sampling.
5. Q_F1,y,y	Energy	Electricity consumption by the destruction process	kWh	(m) measured	monthly	100%	electronic	Project lifetime	Metered
6. Q_F2,y,y	Energy	Steam consumption by the destruction process	kg-steam	(m) measured	monthly	100%	electronic	Project lifetime	Metered



D.5. Relevant data necessary for determining the baseline of anthropogenic emissions by sources of GHG and identification if and how such data will be collected and archived.

Monitored data for baseline emissions (GHG)

ID number	Data type	Data variable	Data unit	Measured (m), calculated (c) or estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/paper)	For how long is archived data kept?	Comment
7. Q_HCFC _y	Mass	The quantity of HCFC 22 produced in the plant generating the HFC 23 waste	tonnes - HCFC 22	(m) measured	monthly	100%	electronic	Project lifetime	Reference data to check cut off condition and rough estimation of Q_HCFC23 _y
8. HFC23_sold	Mass	HFC 23 sold by the facility generating the HFC 23 waste	tonnes -HFC 23	(m) measured	annually	100%	electronic	Project lifetime	Reference data to check cut off condition and rough estimation of Q_HCFC23 _y

**D.6. Quality control (QC) and quality assurance (QA) procedures are being undertaken for data monitored.
(data items in tables contained in section D.3., D.4. and D.5 above, as applicable)**

Data	Uncertainty level of data (High/Medium/Low)	Are QA/QC procedures planned for these data?	Outline explanation why QA/QC procedures are or are not being planned.
1. q_HFC23y	Low	Yes. A QA & QC organization will be formed and QA & QC procedures that are equivalent to JIS (Japanese Industrial Standard) in terms of equipment and analytical method will be set. Will be measured using two flowmeters in parallel with weekly calibration	QA & QC procedures are set and implemented in order to, 1. Secure a good consistency through planning to implementation of this CDM project and, 2. Stipulate who has responsibility for what and, 3. Avoid any misunderstanding between people and organization involved.
2. P_HFC23y	Low	Will be measured using gas chromatography	Ditto
3. Q_NGy	Low	Will be metered using natural gas meter	Ditto
4. ND_HFC23y	Low	Will be measured from the gas effluent of the destruction process	Ditto
5. Q_F _{1,y}	Low	Will be metered using electricity meter	Ditto
6. Q_F _{2,v}	Low	Will be metered using steam meter	Ditto
7. Q_HCFC _y		Will be obtained from production records of the facility where the HFC 23 waste originates	Ditto
8. HFC23_sold		Will be obtained from production records of the facility where the HFC 23 waste originates	Ditto

All of the measurement instruments are to be recalibrated monthly per internationally accepted procedures except for the HFC 23 flowmeters whose recalibration frequency is weekly to reduce the error level.



Miscellaneous parameters

Calculation of the emission reductions also requires data for:

E_{NG_y} - The emissions coefficient for the natural gas used by the destruction process in tonnes of CO₂ equivalent per cubic metre of natural gas (t CO₂e/m³). The value of E_{NG_y} will vary by region and over time.

$E_{F_{i,y}}$ - The emissions coefficient for the electricity used by the destruction process in tonnes of CO₂ equivalent per kWh. The value of $E_{F_{i,y}}$ for electricity depends on the source of the electricity and may vary over time.

$E_{F_{i,y}}$ - The emissions coefficient for the steam used by the destruction process in tonnes of CO₂ equivalent per tonne steam. The value of $E_{F_{i,y}}$ for steam depends on the source of the steam and may vary over time.

GWP_HFC23 - The 100 year Global Warming Potential of HFC 23. The Global Warming Potential converts 1 tonne of HFC 23 to tonnes of CO₂ equivalents (tonnes CO₂e/tonnes HFC 23). The approved Global Warming Potential value for HFC 23 for the first commitment period is 11,700 tonnes CO₂e/tonne HFC 23.